

GMTNIRS and the Promise of High Resolution Spectroscopy in the Infrared: Part 1

Dan Jaffe
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Today:

What is the “infrared”?

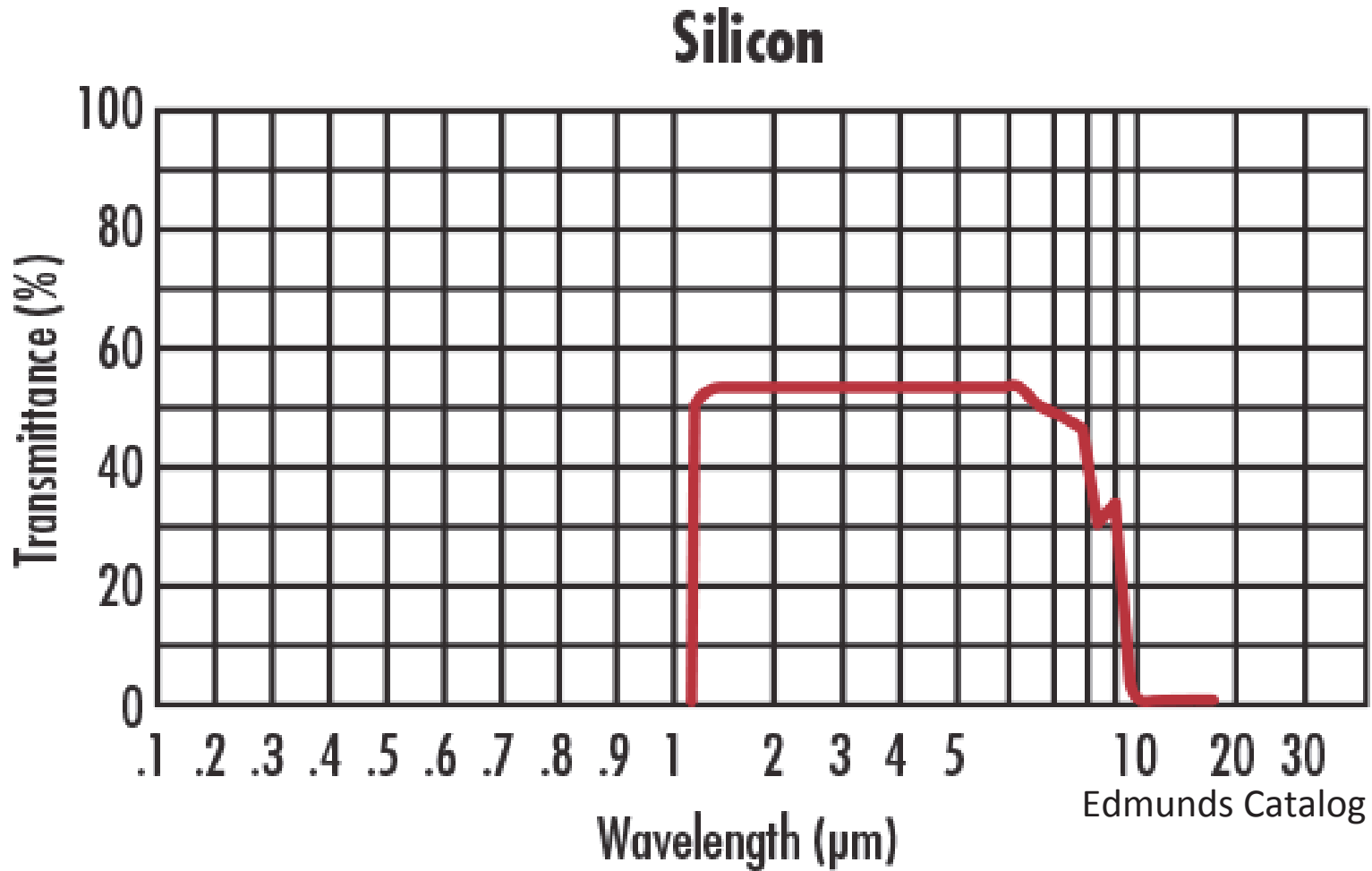
State of the art instruments today

Requirements and where they come from

GMTNIRS

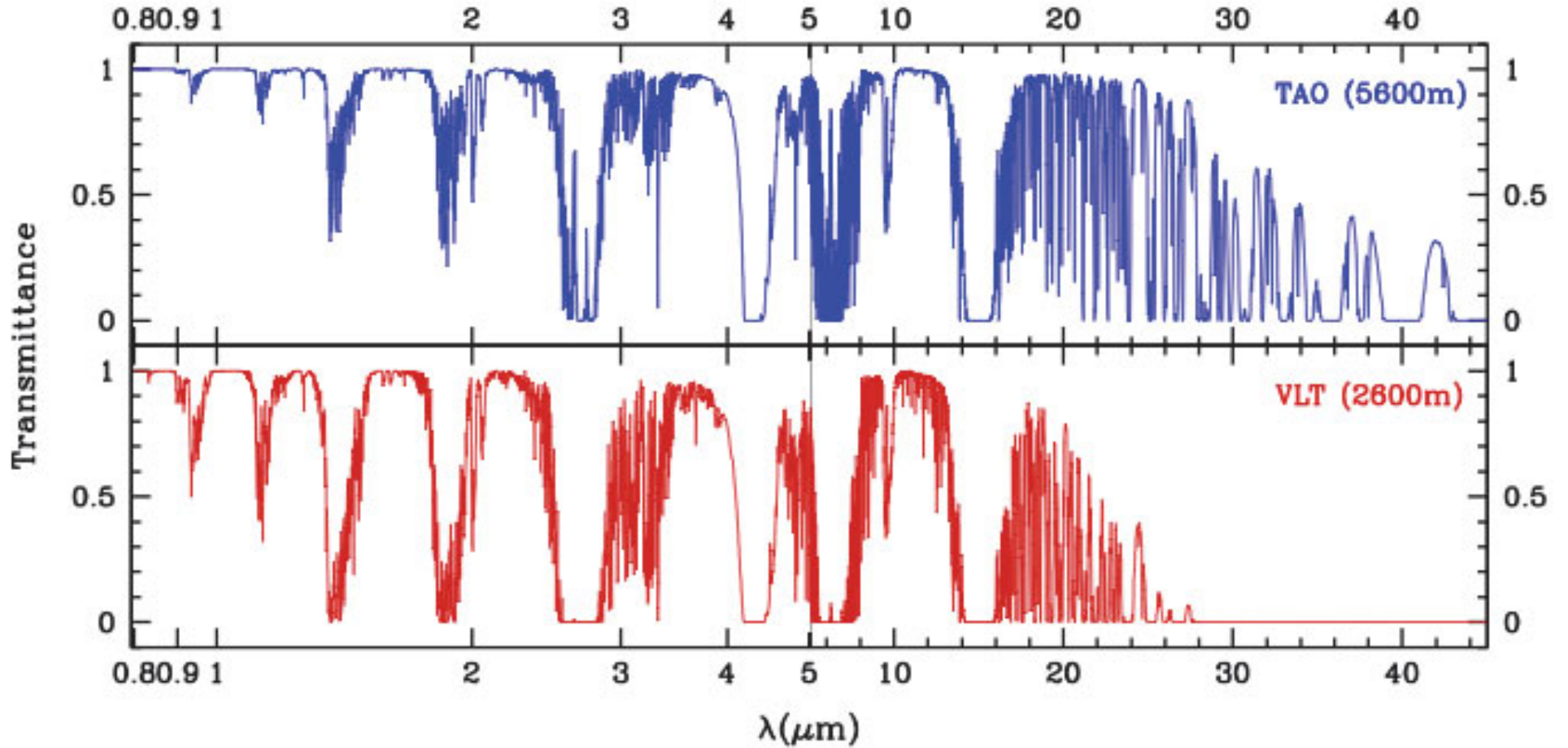
Spectrograph basics

Immersion gratings- the “secret sauce”



Dominant IR options are HgCdTe or InSb, both with Si multiplexers.

The infrared divides into windows



University of Tokyo Observatory

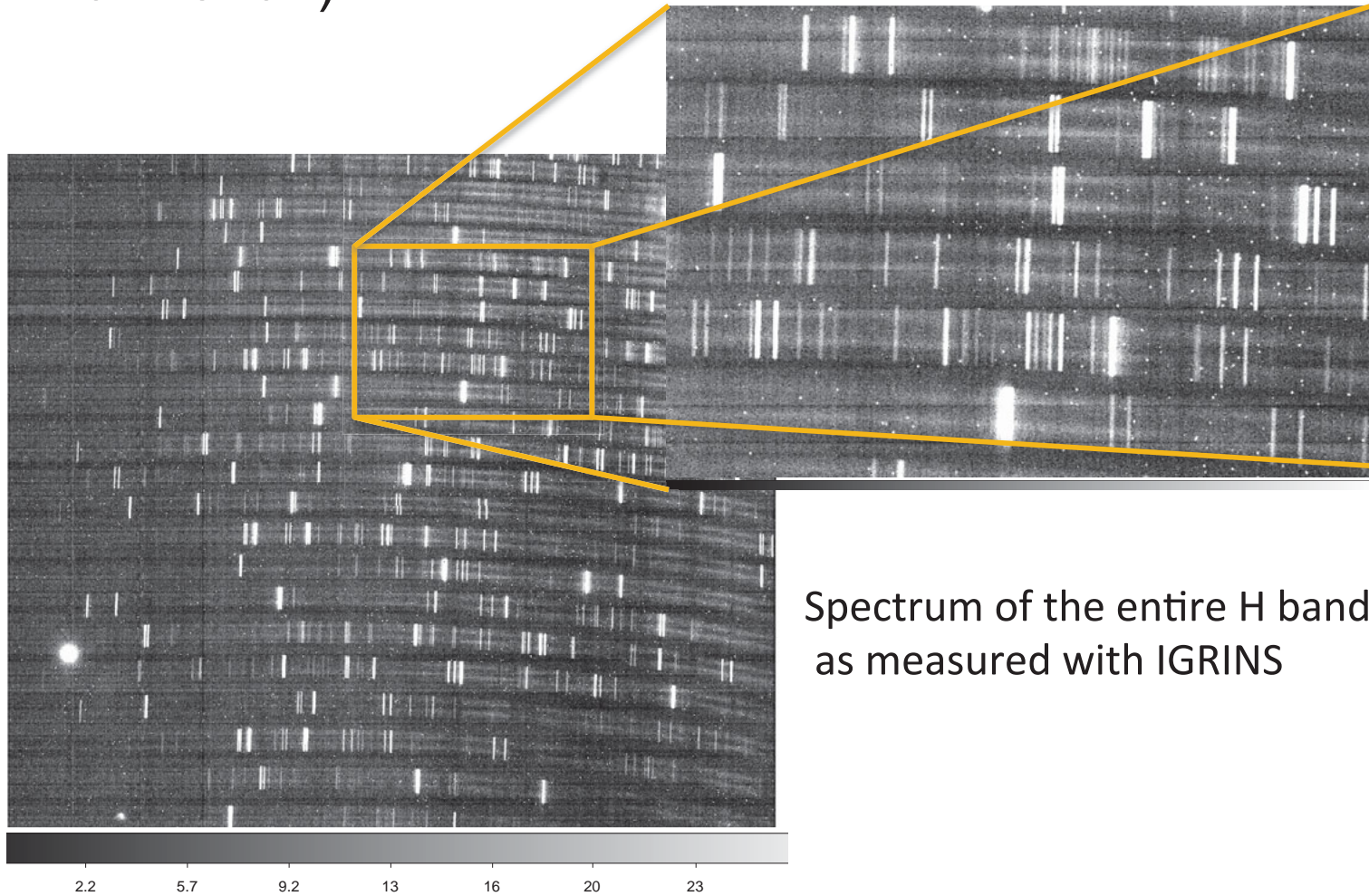
Background from Sky

$$N = B_{\nu} \Delta\nu A \Omega_{\text{pix}} \epsilon / (h\nu)$$

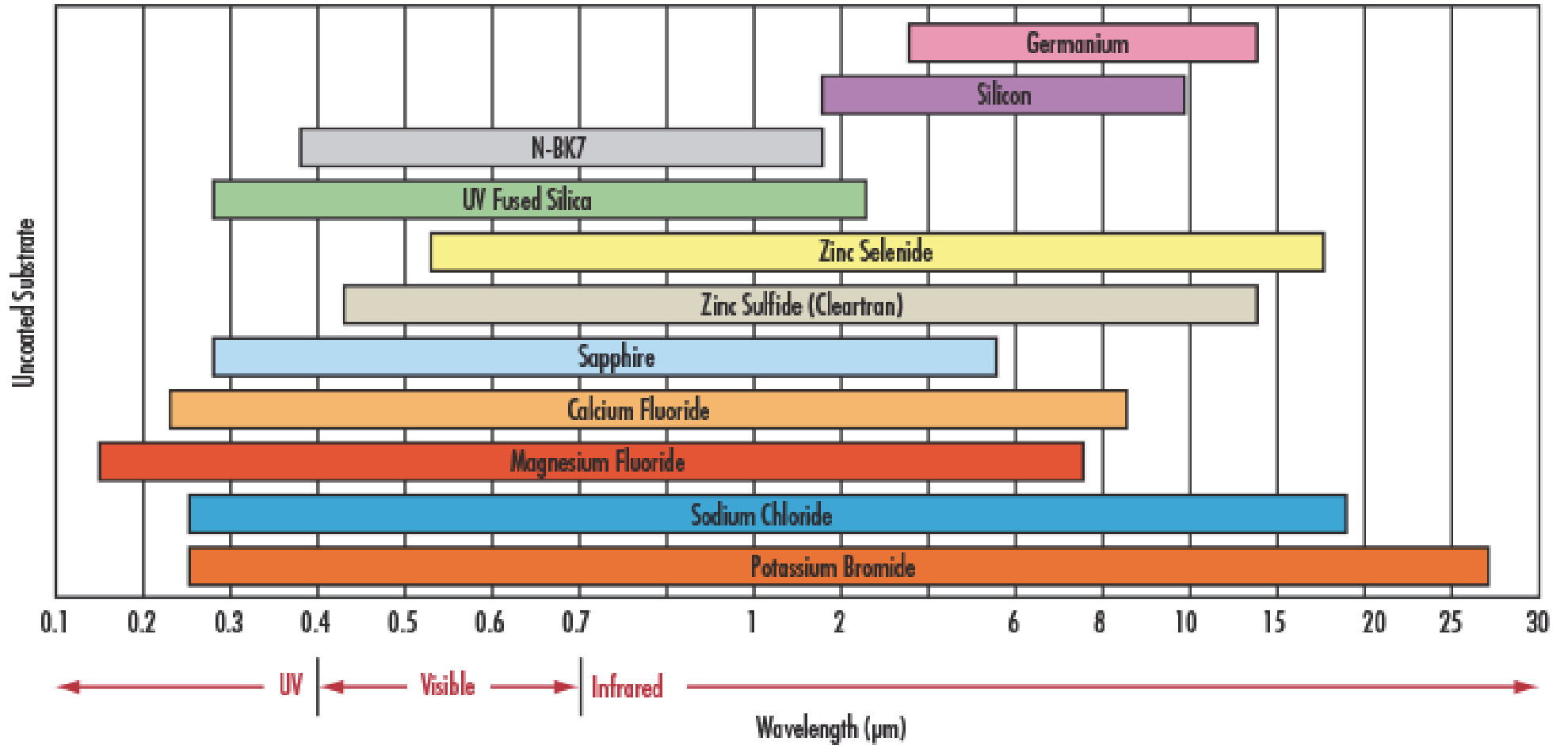
GMTNIRS Background Counts e/s/pixel

J	H	K	L	M
5e-10	6e-6	1e-2	8	342

OH Night sky in the H band (Chan Park et al.)



Spectrum of the entire H band
as measured with IGRINS



State of the art instruments today

Resolving power and resolution

$R = \lambda / \Delta\lambda$ Resolution = $\Delta\lambda$ or in some cases ΔV

Coverage angstroms, nm, μm –take your pick.

Note Window widths: H and K are each ~ 400 nm
or about $\lambda/5$

First-generation high resolution spectrographs for the IR

Small wavelength coverage:

CSHELL: $\lambda/200$

Phoenix: $\lambda/100$

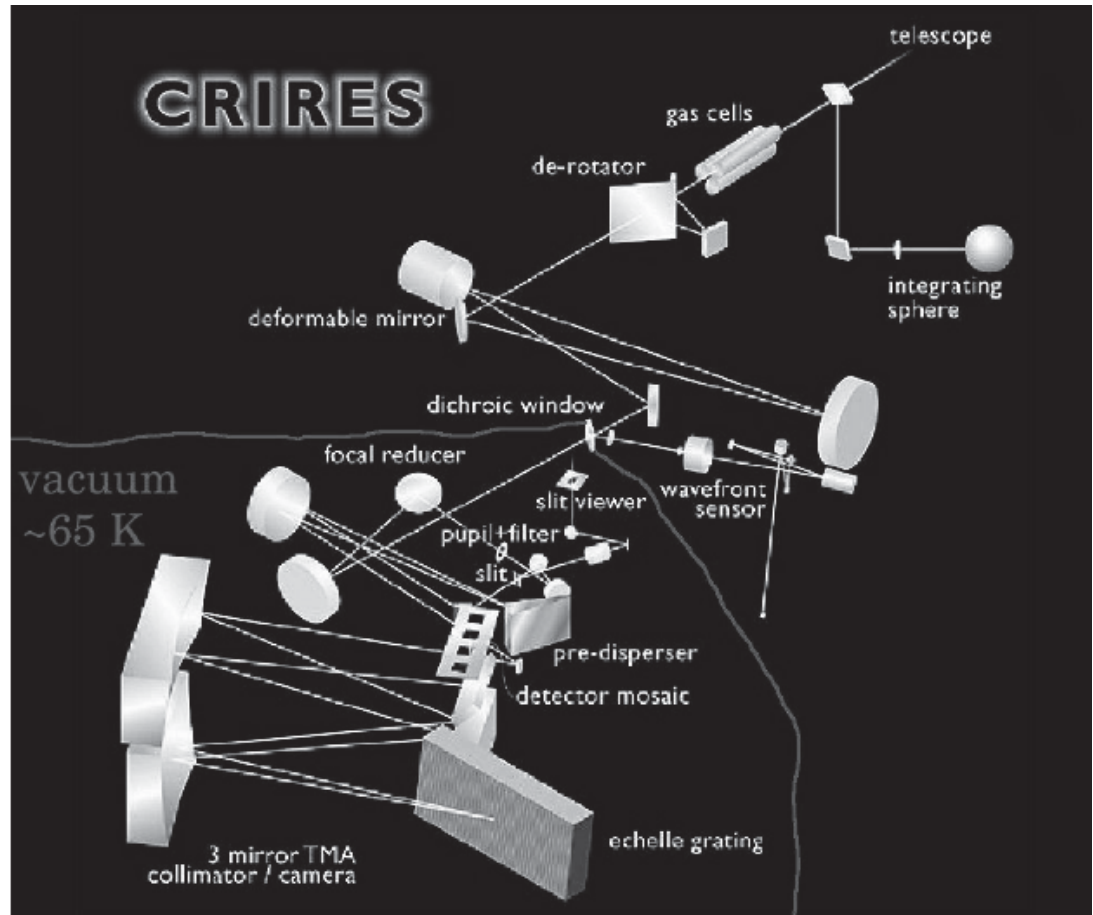
CRIRES: $\lambda/70$

Small coverage means lots of moving parts.

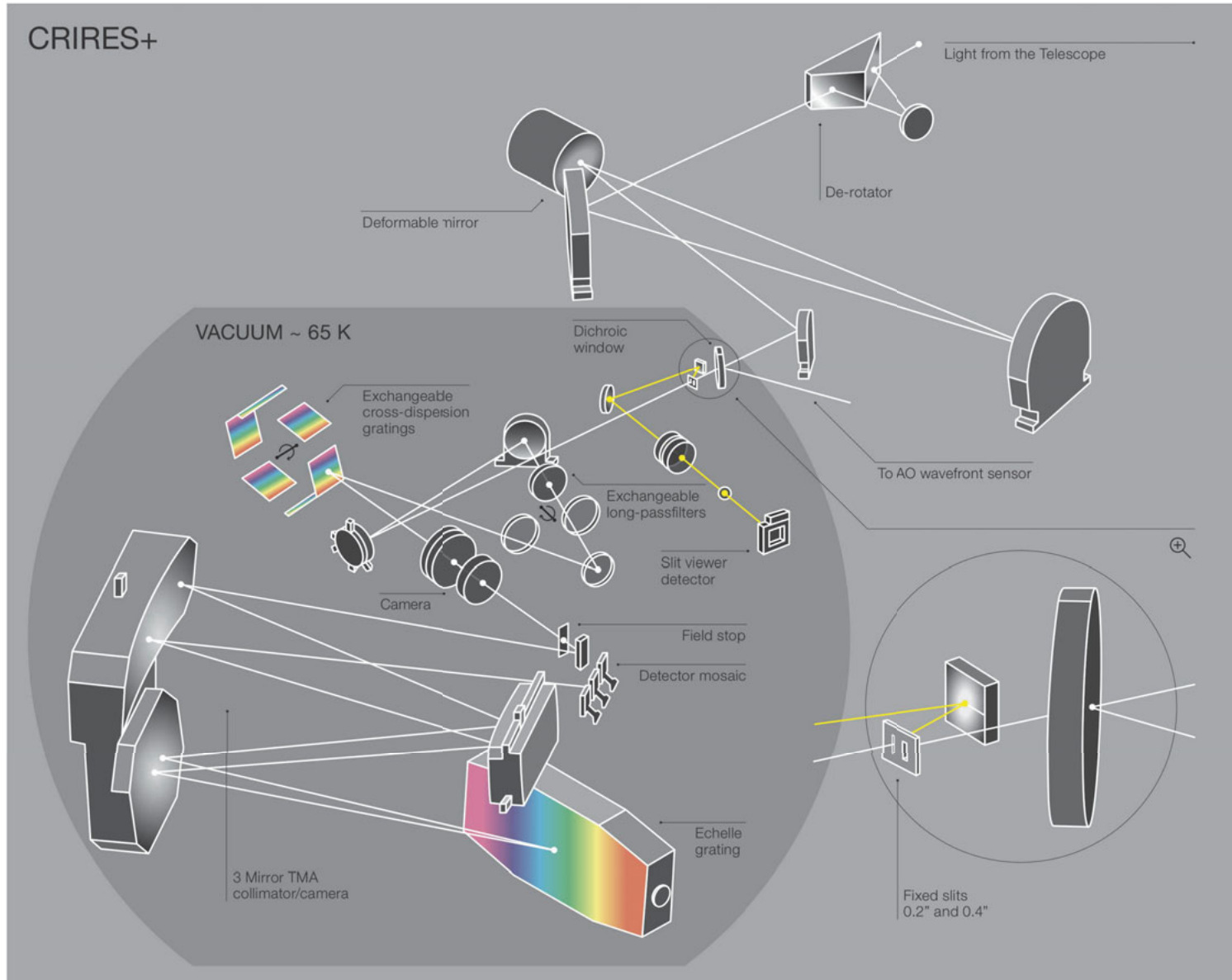
Many surfaces.

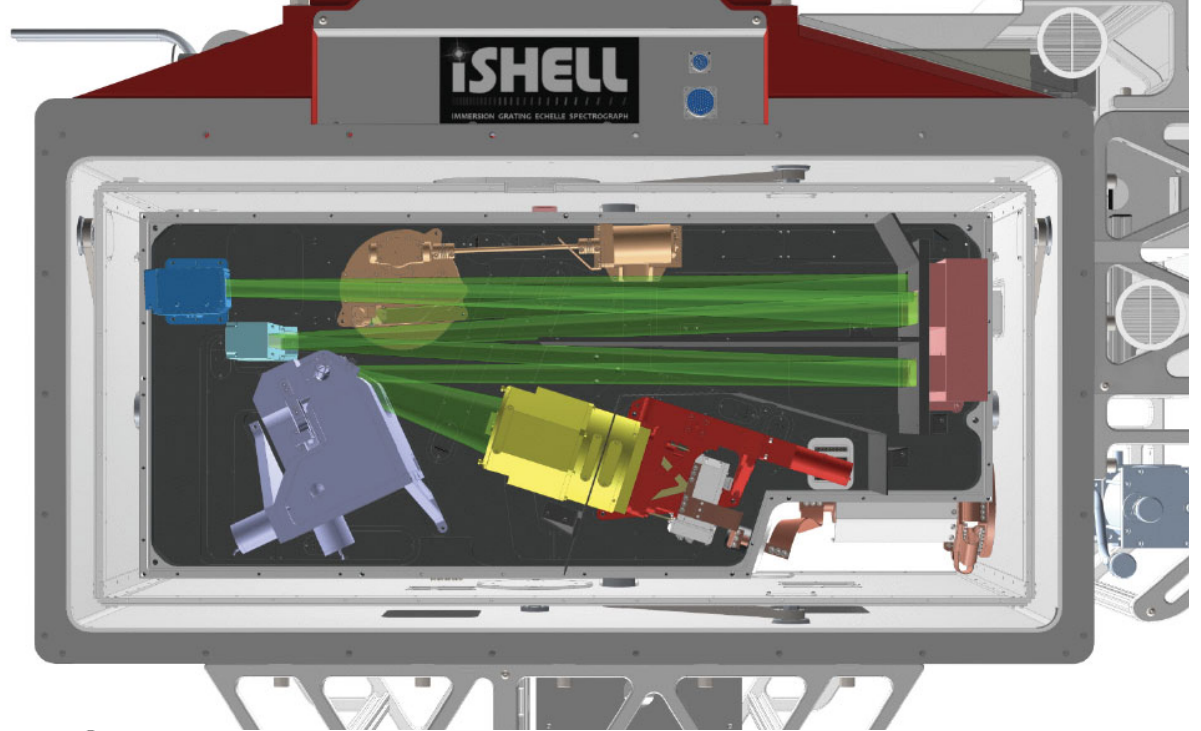
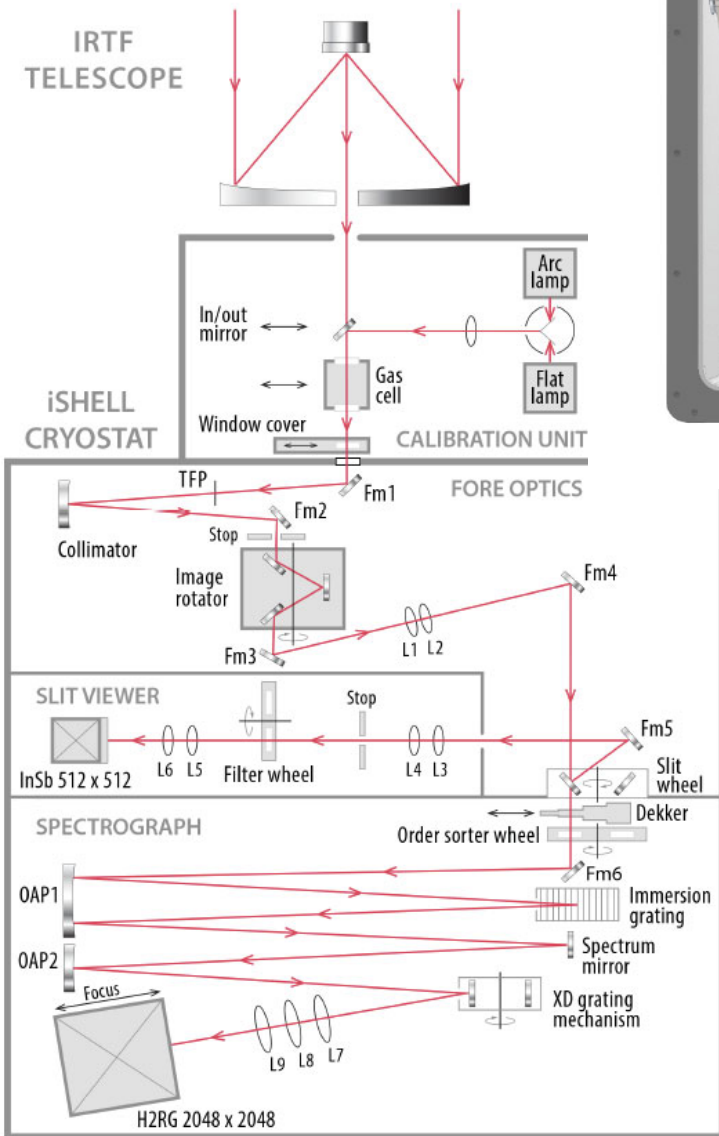
Hard to get decent slit sizes at high resolution.

Instruments already quite large and so not too stiff.



VLT CRIRES+ - Full coverage of K





iSHELL on the NASA IRTF

R=70,000 1-5 μm in snippets

Resolving power
Spectral coverage
Detector,
Background
Throughput
Sampling
Slit length
Spatial resolution,
Spectral stability
Stability overall

Resolving power

Science driven and technology limited.

$$R_{\text{Diff}} = 2W \tan \beta / \lambda$$

You are limited by the size of the grating and the need to let light into your system. Let's look at the S/N aspects.

Let's fix the number of pixels per resolution element:



How does S/N scale with R?

		Short I (low bknd)	Long I (high bknd)
Low S/N (=>detector noise limit when background is low)	Continuum	$1/R$	$1/\text{SQRT}(R)$
	Unresolved	Independent of R	$\text{SQRT}(R)$
	Resolved	$1/R$	$1/\text{SQRT}(R)$
	Emission unresolved	Independent of R	$\text{SQRT}(R)$
High S/N	Continuum	$1/\text{SQRT}(R)$	$1/\text{SQRT}(R)$
	Unresolved	$\text{SQRT}(R)$	$\text{SQRT}(R)$
	Resolved	$1/\text{SQRT}(R)$	$1/\text{SQRT}(R)$
	Emission unresolved	Independent of R	$\text{SQRT}(R)$

Which regimes matter?

		Short I (low bknd)	Long I (high bknd)
Low S/N (=>detector noise limit when background is low)	Continuum	1/R	1/SQRT(R)
	Unresolved	Independent of R	SQRT(R)
	Resolved	1/R	1/SQRT(R)
	Emission unresolved	Independent of R	SQRT(R)
High S/N	Continuum	1/SQRT(R)	1/SQRT(R)
	Unresolved	SQRT(R)	SQRT(R)
	Resolved	1/SQRT(R)	1/SQRT(R)
	Emission unresolved	Independent of R	SQRT(R)

What if you bin?

Spectral coverage: Which wavelengths?

Short IR

Thermal IR

Mid-IR

Spectral coverage: Grasp

Enough to cover line of interest

Enough to cover group of lines of interest

Enough to cover band or bands

Pan-spectral coverage enables a new mode of science for the infrared

Detector

Quantum efficiency: As high as possible

Read noise: Below reasonable backgrounds or as low as possible

Dark current: Below reasonable backgrounds or less than read noise in reasonable exposure times.

Wavelength coverage: to as long as necessary but not longer

Readout speed: Not too slow (Fowler sampling)

Size: Big

Pixel Pitch: People may disagree but not small at long λ

Memory and cross-talk: As little as possible

Well depth: Big enough to allow high S/N per exposure

Linearity: Good over full range or calibratable

Internal background: Basically a requirement on how cold your internal optics need to be.

Has to be less than dark current plus external background at the shortest wavelength you observe with a given channel.

Why do I phrase it that way?

External Background

Good site

As few external surfaces as possible

Cut off where atmosphere or detector does

Cold stop- Must rotate

The trade for AO- more surfaces vs. smaller $A\Omega$

Slit losses vs. Strehl

Requirements and where they come from

Throughput: Obviously more is better. This is particularly true at short wavelengths where you will be source noise or detector noise limited. It matters somewhat less at longer wavelengths where cold throughput affects signal and background both- This tells you which channels to concentrate on.

Sampling: A combined real estate and noise question. You want to sample enough that your slit or diffraction are limiting R but oversampling takes up pixels you could use for slit length or spectral coverage and more pixels/resel means higher read noise to overcome.

For high resolution IR spectroscopy, the sweet spot lies between 2.5 and 4 pixels per resolution element.

Slit length: Needs to be long enough to allow sky subtraction by switching along the slit while always having the object in it.
=>Depends on seeing or AO.

Planetary astronomy and ISM work want to drive you to longer slits.

Spatial resolution: Why?

ISM, Planets, disks, binaries, confused regions, exoplanets

Limiting Factors:

Seeing- go to AO

Diffraction

Pixel size

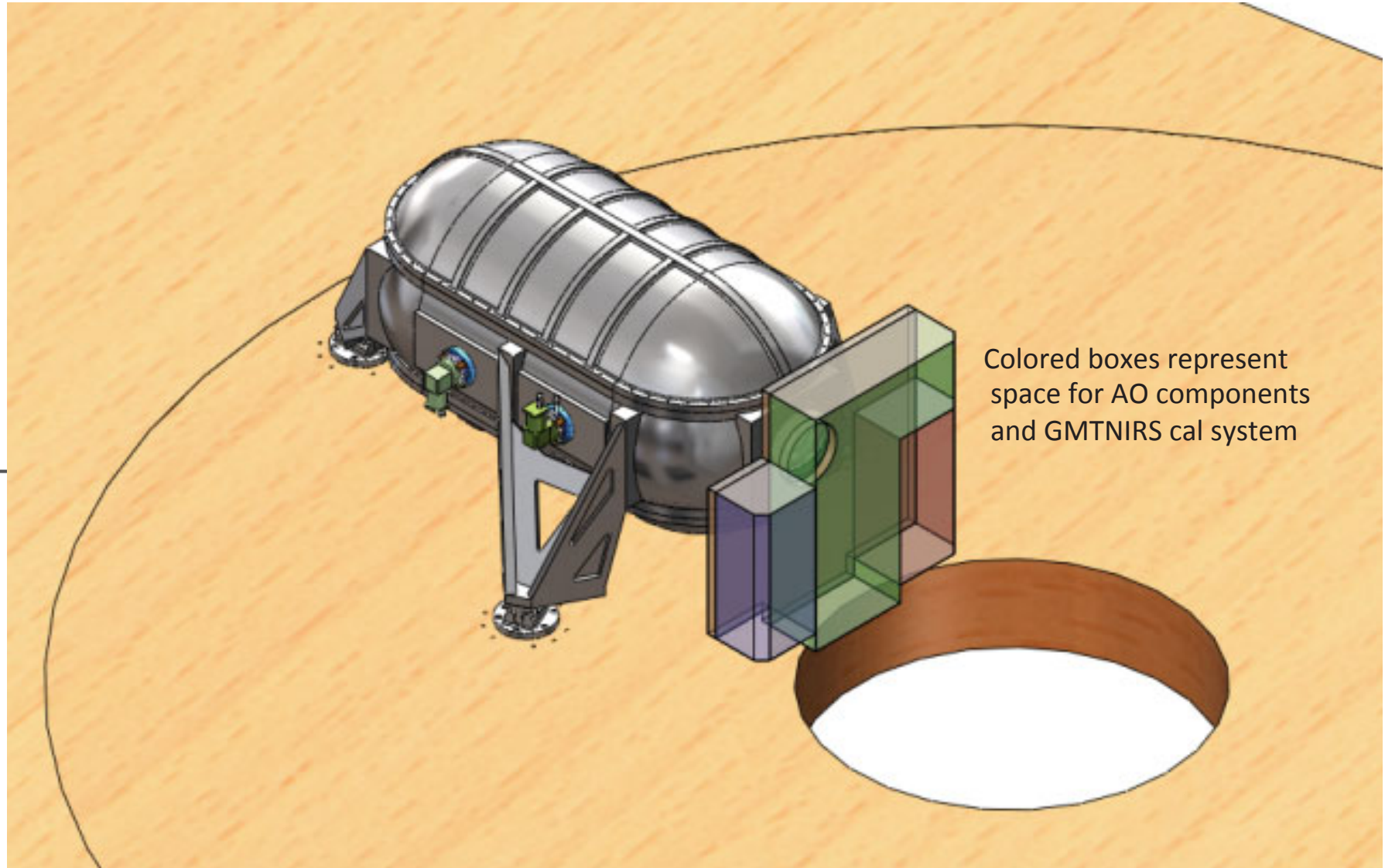
Image wander

Spectral stability: Depends on application. Achievable by mechanics, calibration, or both.

Stability overall: Helps data reduction, calibration. Allows for higher limiting S/N

- Covers all spectrum transmitted by the atmosphere from 1.07 μm to 5.3 μm in a single exposure.
- Resolving power 65,000 at $\lambda < 2.5 \mu\text{m}$, 85,000 at $\lambda > 2.9 \mu\text{m}$.
 - 65 mas slit, 1.3" long
 - No moving parts after slit
 - High throughput leads to high sensitivity
 - K-band slit viewing camera
 - Automated, near publication quality data pipeline

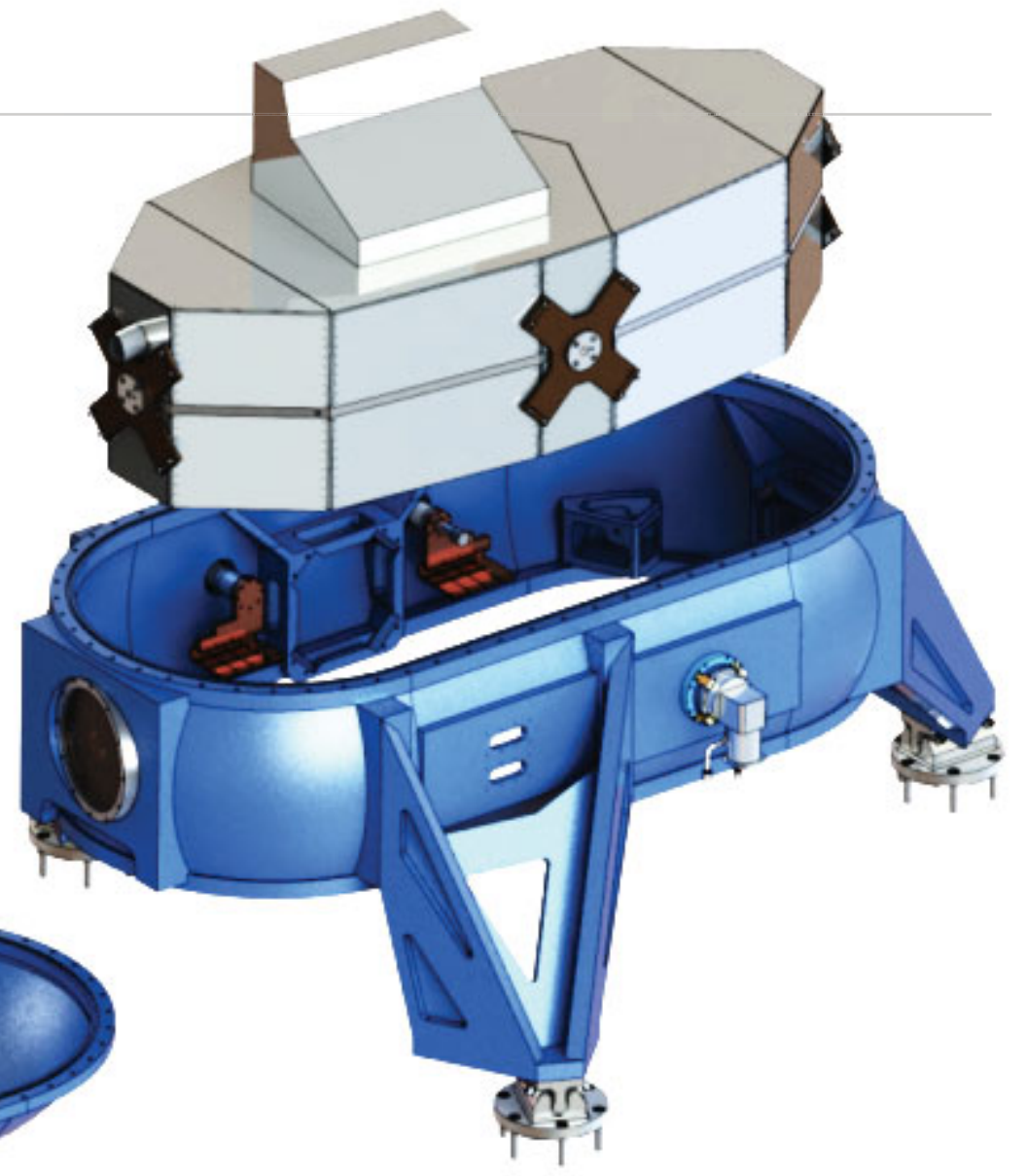
GMTNIRS on rotating instrument platform





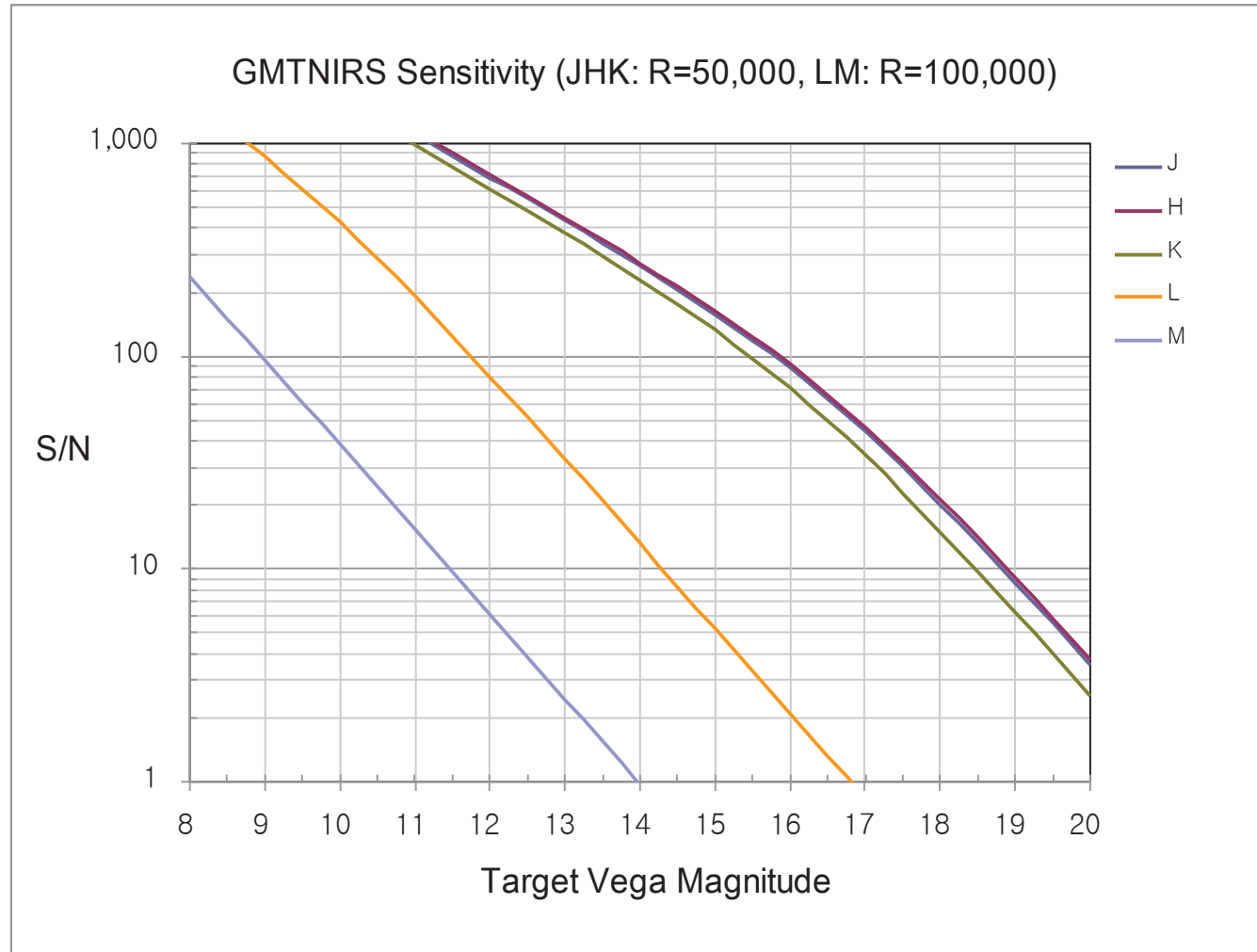
TEXAS

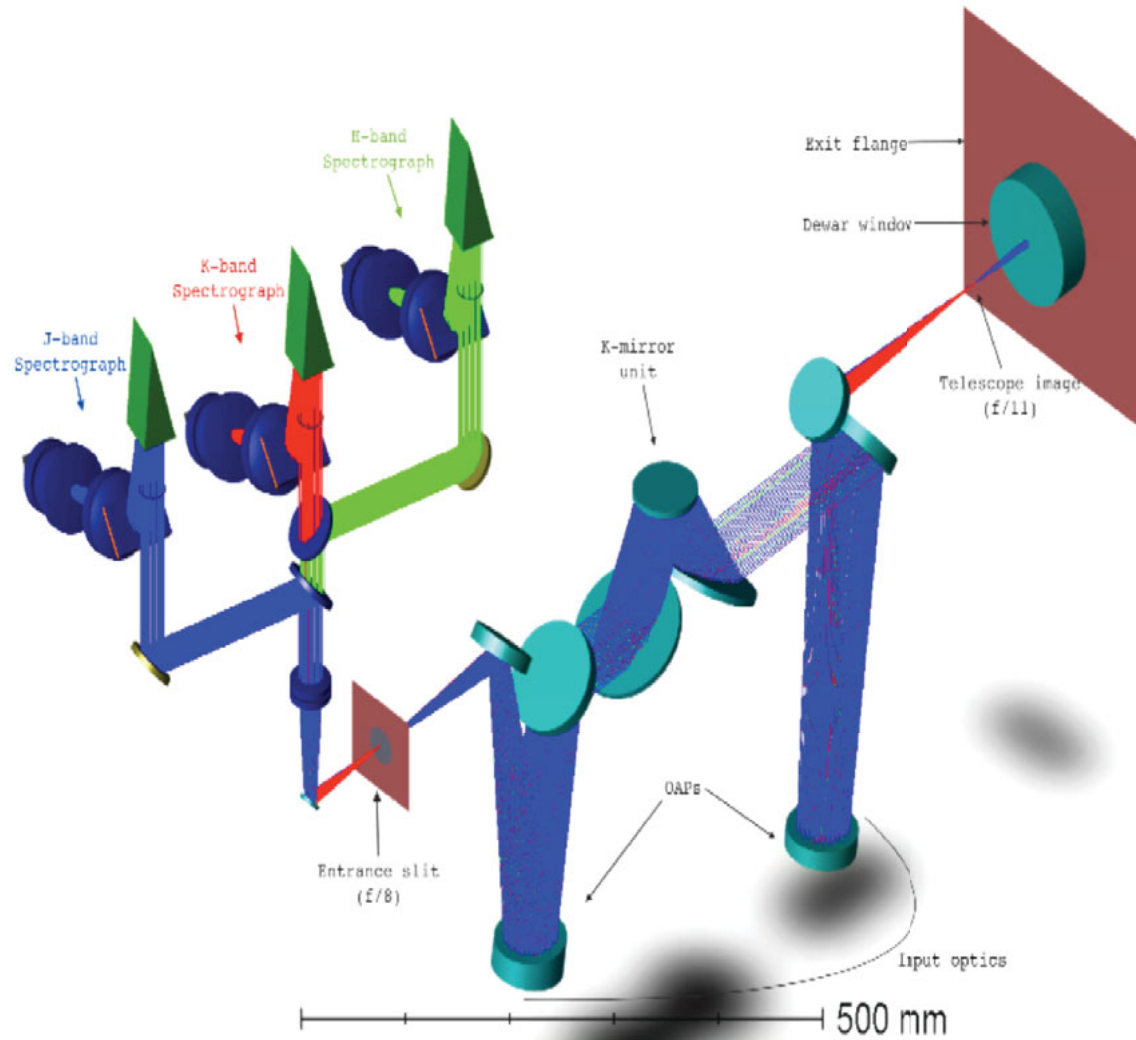
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GMTNIRS sensitivity calculated conservatively: Average position along the blaze of both the echelle and the cross-disperser, 6x600 second exposures, image size = slit size.

In J,H,K, GMTNIRS can take a $S/N > 100$, $R=50,000$ spectrum of basically anything in the 2MASS catalog in under an hour

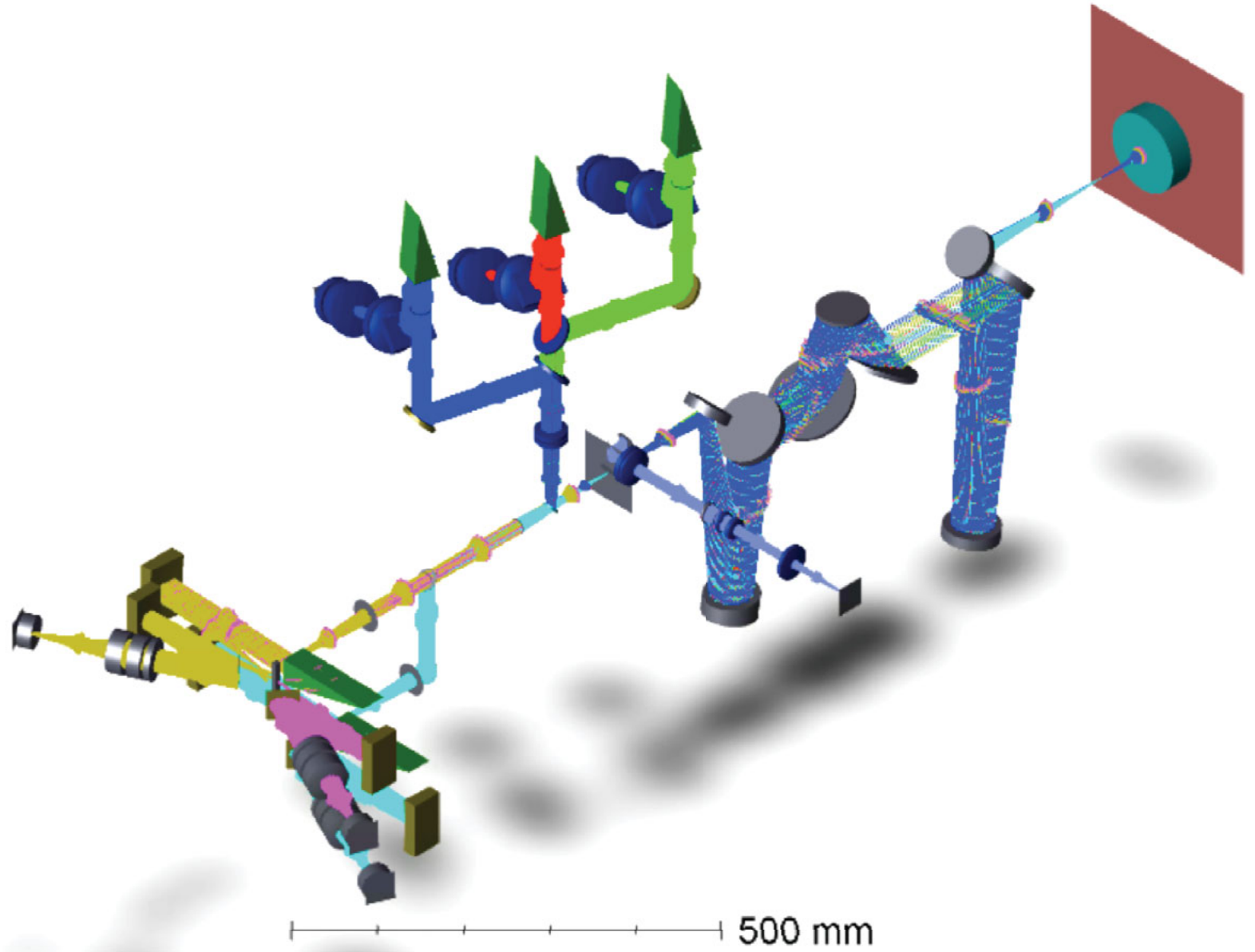






TEXAS

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Spectrograph basics: Spectrograph design without the grating equation:

$$R_{\text{diff}} = Nm$$

#of diffraction limited resels/order = # of grooves

Diffraction limited spot size at focal plane = $f \cdot \lambda$

Diffraction limited spatial and spectral spot sizes the same.

Real resolving power:

$$R = R_{\text{diff}} \cdot (\theta_{\text{diff}} / \theta_{\text{slit}}) = Nm (\lambda / D) (\theta_{\text{slit}})^{-1}$$

(where in the right-hand version θ_{slit} is in radians)

Let's design a spectrograph that can cover the entire K band (2.0-2.5 μm) in a single exposure at $R=50,000$ for use on GMT.

Givens:

Detector is 2048x2048 with 18 μm pixels (standard Teledyne product)

Diffraction limit of telescope = $0.08 * 2.2 = 18$ mas.

We need a slit of 70 mas (this is about $4\lambda/D$)

This protects against phase errors and image wander, allows long wavelength use of same slit.

Let's also decide that we want to sample with 4 pixels per slit width.

Trial Spectrograph Design (use these rules)

The $4\lambda/D$ slit implies that $R_{\text{diff}}=200,000$ to get $R=50,000$

With 4 pixel sampling $R_{\text{perpix}} = 4 \times 50,000 = 200,000$

The two together mean that $R_{\text{perpixel}} = 200,000$ or λ/D
i.e. one R_{diff} for each pixel.

This also means that each pixel is one diffraction limited spatial element, or 18 mas.

Because of the length of a free spectral range varies across the band, we cannot use the full detector width at 2.2 microns. Better to use about 80% or 1600 pixels.

So, **N=1600 grooves** which will make the 2.2 μ m order free spectral range cover 1600 pixels.

How long does the grating have to be?

$$R_{\text{diff}} = 200,000. \quad L = \lambda R_{\text{diff}} / (2 \sin \delta)$$

For reasonable values:

$$L = 2.2 \times 10^{-4} \cdot 2 \times 10^5 / (1.8) = 24 \text{ cm}$$

What is the groove pitch we need?

$$2.4 \times 10^{-1} / 1600 = 1.6 \times 10^{-4} \text{m} = 160 \mu\text{m} \Rightarrow 6 \text{ grooves/mm}$$

THIS IS IMPOSSIBLY COARSE

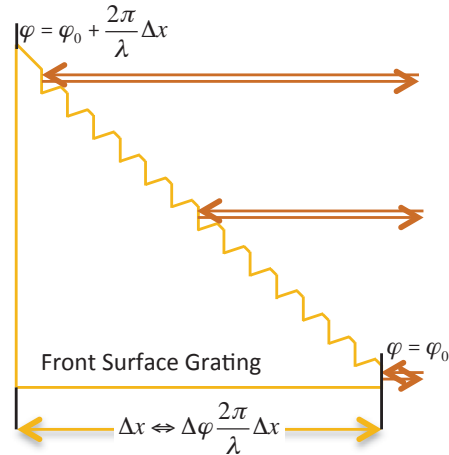
What camera f/ number do we need?

f/λ needs to equal the pixel size of $18 \mu\text{m}$,
so we need f/8. THIS IS PRETTY EASY.

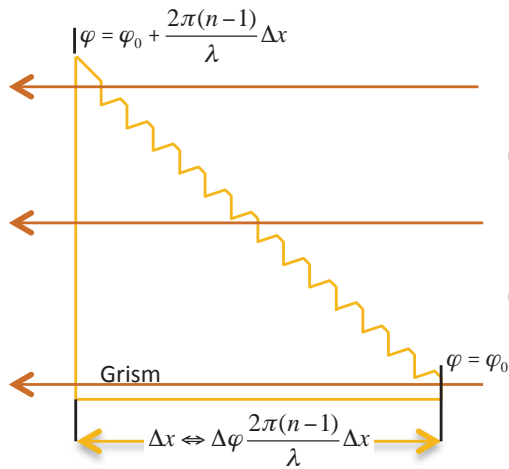
Now, the only question is the cross-dispersion.

The window is about $\Delta\lambda/\lambda = 0.22$, so we need $0.22 * 50,000 = 11,000$ individual resolution elements. Our central order has 400 elements, so we need 28 orders. If we spread these across 2000 pixels, we have 71 pixels per order for a mean separation of $0.018 * 71 = 1.3''$.

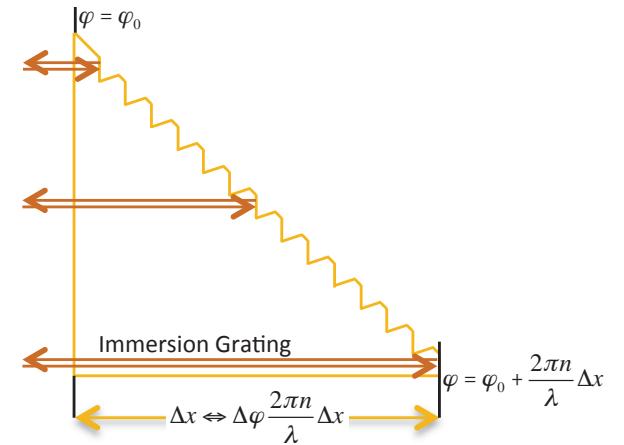
In practice, we will need to leave some space between orders so the slit length will be closer to 1". Good thing this is an AO instrument.



$n_{Si} \sim 3.4$



(see our grism instrument design paper: Deen et al. (2017), PASP)



Resolving power is equal to phase delay across the beam measured in wavelengths divided by the ratio of the angular size of the slit to the diffraction limited angular scale.

$$R = \lambda/\Delta\lambda = (2L\sin\delta)/\lambda \cdot \theta_{\text{diff}}/\theta_{\text{slit}}$$

Where L is the grating length and δ is the grating angle.

In immersion, the internal wavelength shrinks by a factor of n, the refractive index

$$m\lambda = n_G \sigma (\sin \alpha + \sin \beta)$$

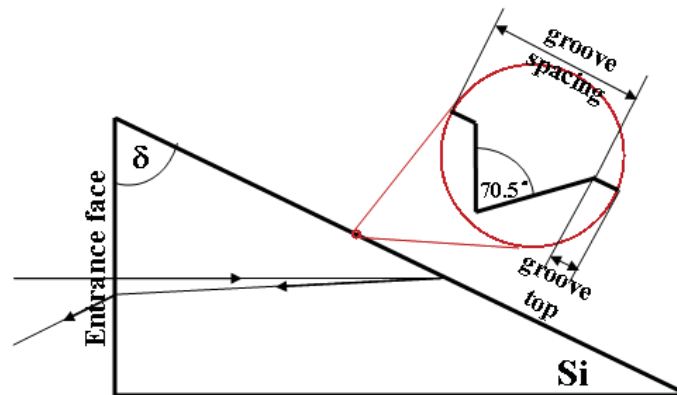
$$R_{\text{max}} = \frac{2n_G L \sin \delta}{\lambda}$$

$$\frac{d\beta}{d\lambda} = \frac{2n_G \tan \beta}{\lambda}$$

The invention of the immersion grating by Dan Jaffe

1. The “eureka moment”- Spring 1992

If you illuminate a grating from inside a transparent medium, the density of the medium leads the light to see the grating as “longer”, that is, bigger by a factor of the refractive index, n , which is 3.4 for silicon



The invention of the immersion grating by Dan Jaffe

2. The “oh” moment – discovering a US patent from 1984

United States Patent [19] [11] **Patent Number:** 4,475,792
Sica, Jr. [45] **Date of Patent:** Oct. 9, 1984

[54] **HIGH RESOLUTION DIFFRACTION GRATING**

[75] **Inventor:** Louis Sica, Jr., Alexandria, Va.

[73] **Assignee:** The United States of America as represented by the Secretary of the Navy, Washington, D.C.

[21] **Appl. No.:** 402,403

[22] **Filed:** Jul. 27, 1982

[51] **Int. Cl.** G02B 5/18

[52] **U.S. Cl.** 350/162.17; 350/162.22; 350/162.23; 356/305

[58] **Field of Search** 356/305, 328, 302, 331-334; 350/162.17, 162.2, 162.21-162.23

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Aoyagi et al., *Optics Communications*, vol. 29, No. 3, Jun., 1979, pp. 253-255.

Hugh L. Garvin, E. Garmire, S. Somekh, H. Stoll and A. Yariv, "Ion Beam Micromachining of Integrated Optics Components" *Applied Optics*, vol. 12, No. 3; Mar., 1973; pp. 455-459.

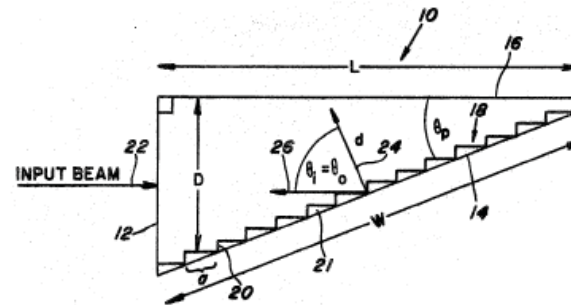
E. G. Loewen, M. Neviere and D. Maystre "Grating Efficiency Theory as it Applies to Blazed and Holographic Gratings" *Applied Optics*, vol. 16, No. 10; Oct., 1977 pp. 2711-2721.

Primary Examiner—F. L. Evans
Attorney, Agent, or Firm—Robert F. Beers; William T. Ellis; Charles E. Krueger

[57] **ABSTRACT**

An optical prism, with an input surface, a reflecting surface and a base, and with a diffraction grating formed on the reflecting surface. The prism is designed so that if an input beam is incident normal to the input surface, then the efficiency of the order diffracted in the direction opposite the input beam is greater than a predetermined value. If the prism is fabricated of a material with index of refraction n , then the resolving power of the grating is increased by n .

8 Claims, 6 Drawing Figures



The invention of the immersion grating by Dan Jaffe

3. The “hah” moment- finding an article from Nature, 1954

NATURE March 6, 1954 Vol. 173

EDITORS

whose responsibility
is correspondence
is communications

**and Angle in
anies**

The accepted theory
of aberrations is very
in cases. You give
L. Its state function
of the co-ordinates
specimen, contains
of the shape of
connected with any
typical location. Let
If you measure its
with this measure-
but only operators
is not meaningful,
the last question is
the between the 2nd
h. Let L be a sym-
ple variable z , the
of its arguments.
very; for example,
function of the three
the half-wavelength

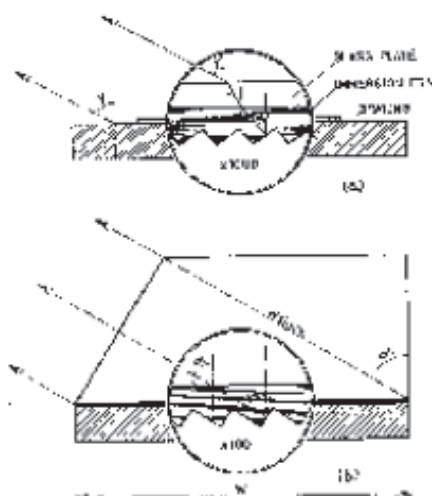


FIG. 1

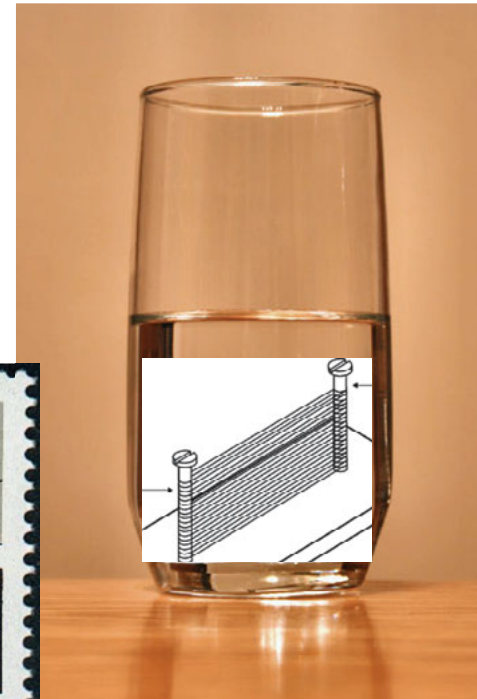
so that of the immersion microscope, was further
developed in accordance with Figs. 1a and 1b.
If we bring a plane of convergence with optical

The invention of the immersion grating by Dan Jaffe

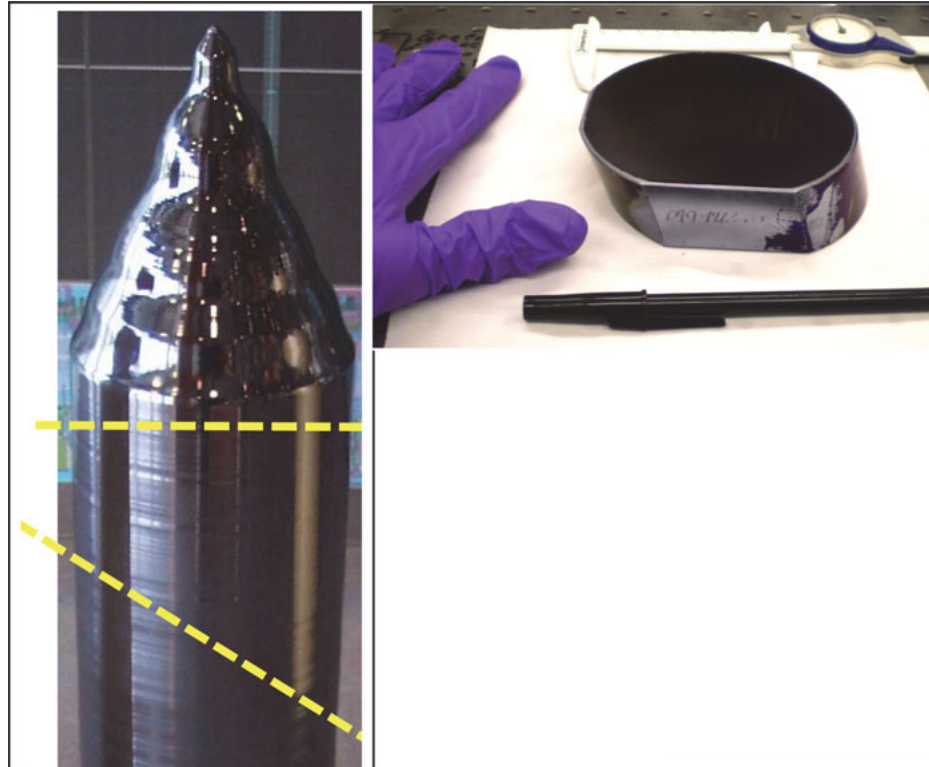
4. The “duh” moment: *Gegenseitige Einwirkung der im Wasser und anderen brechenden Mitteln gebeugten Strahlen* Joseph Fraunhofer 1823

The interaction of diffracted radiation in water and other refractive media.

Fraunhofer immersed his gratings in water, linseed oil, and turpentine. We immerse ours in solid silicon but the physics is the same.

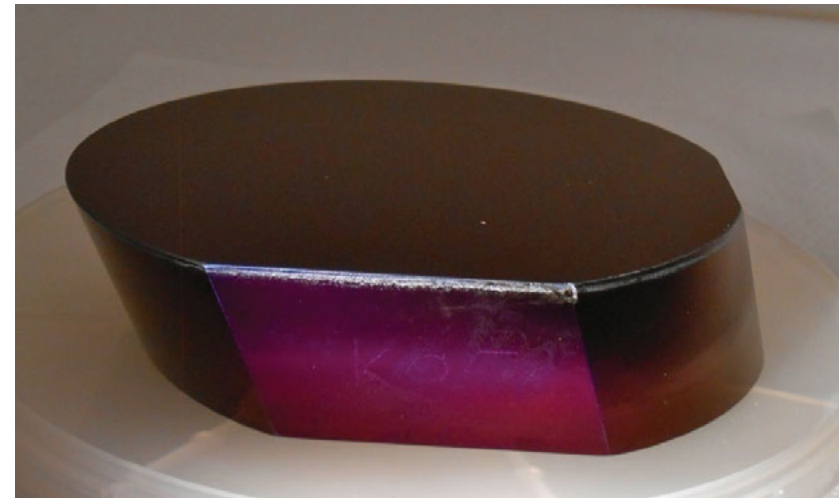


The thick substrates require a completely independent process chain from what wafers require.

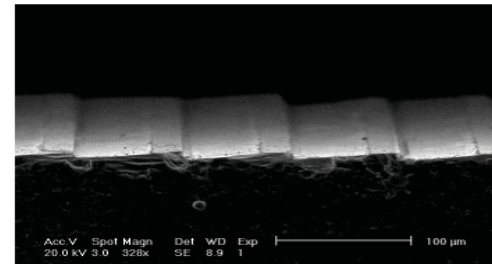
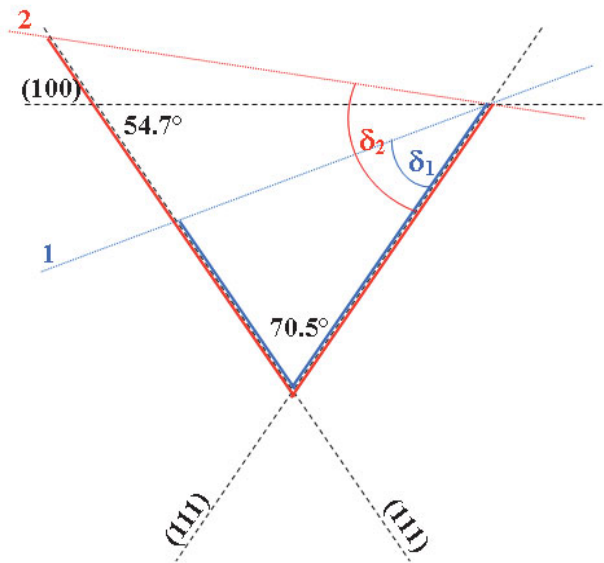


Material preparation requires coordination of:

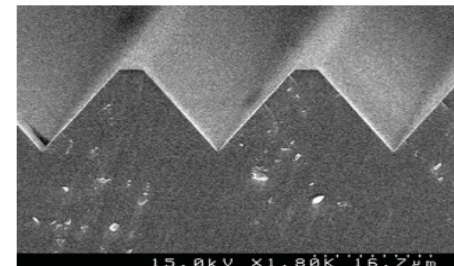
1. Float-zone silicon boule, resistivity of $>10,000$ ohm-cm.
2. X-ray crystallography to orient to 0.04° . Tilt and slice boule.
3. Chemically mechanically polished to $\lambda/10$
4. LP-CVD silicon nitride $600 \text{ \AA} \pm 5\%$



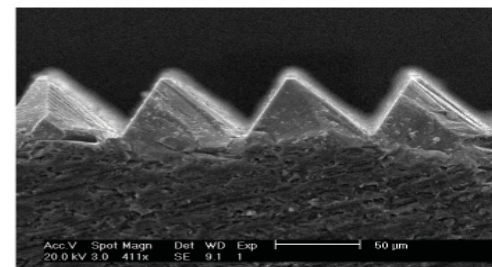
By correctly orienting the disk surface with respect to the silicon crystal planes, we can produce a grating with any blaze angle.



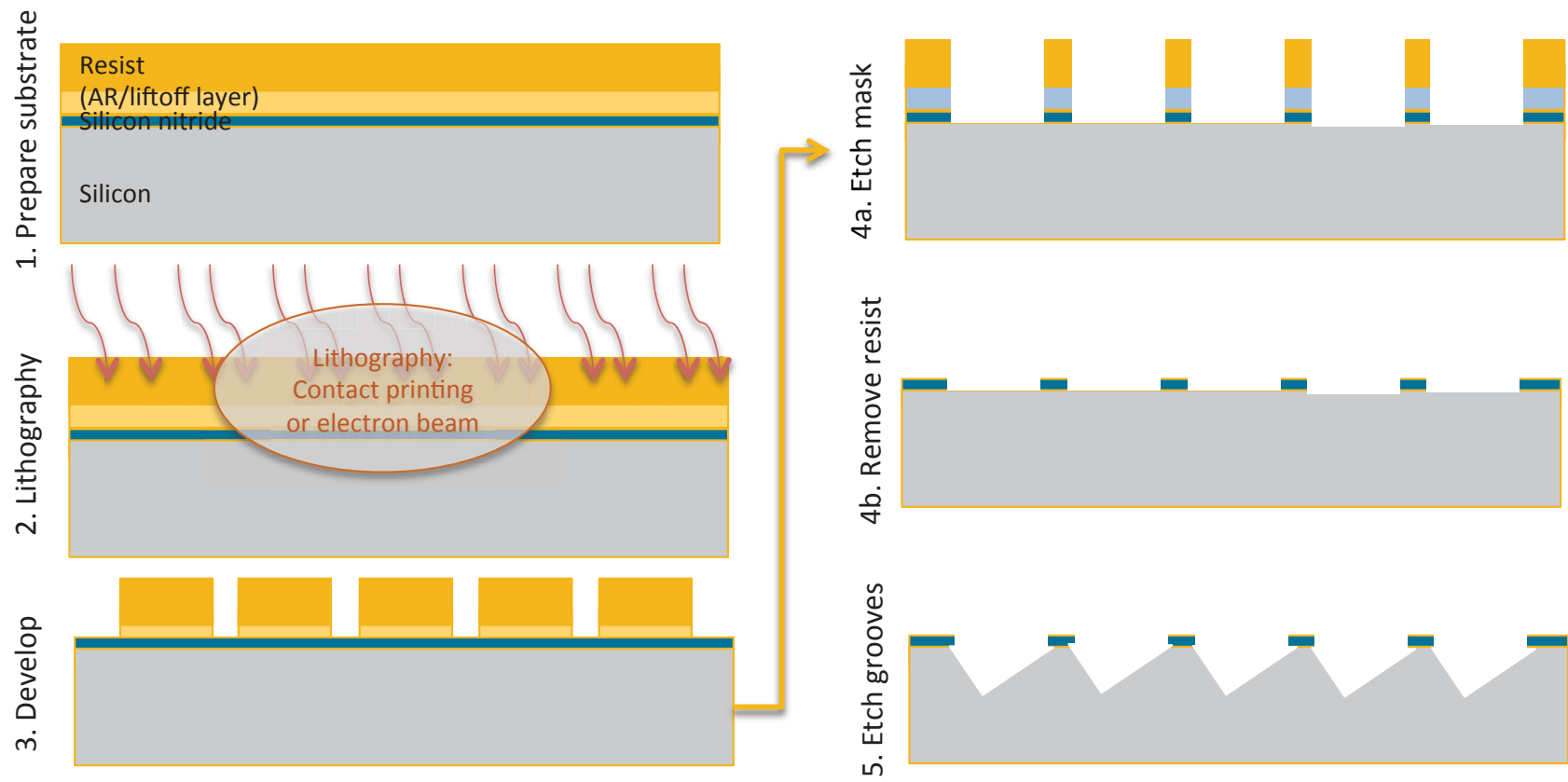
6.16°

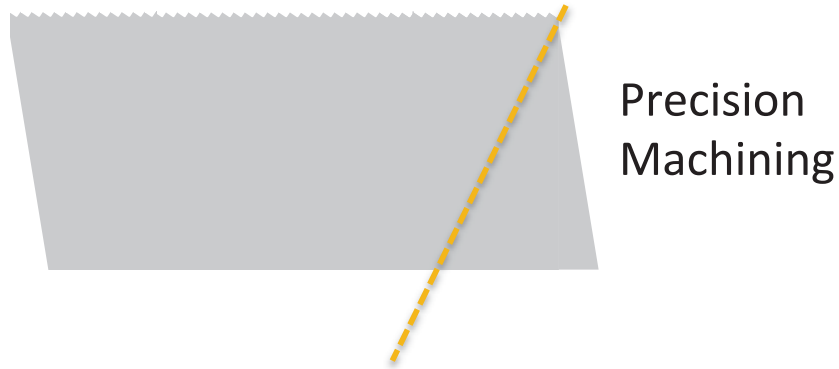


54.7°

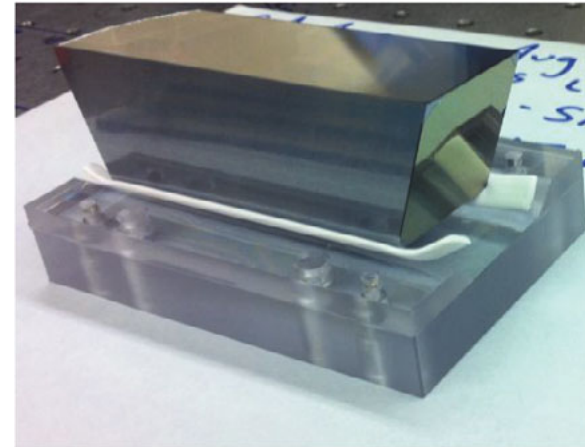
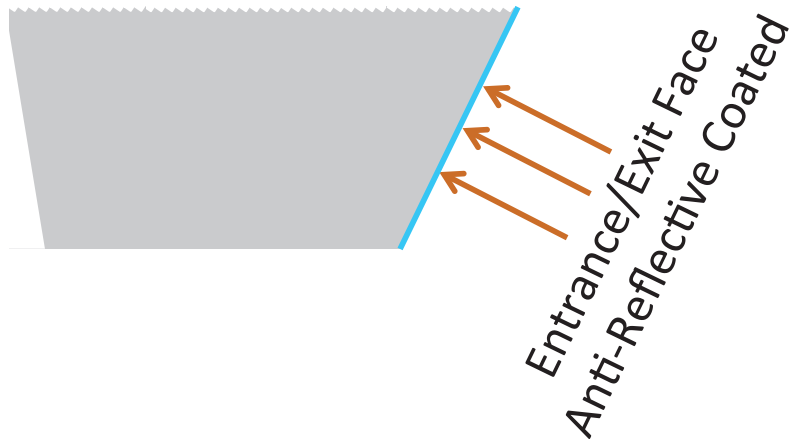


63.4°



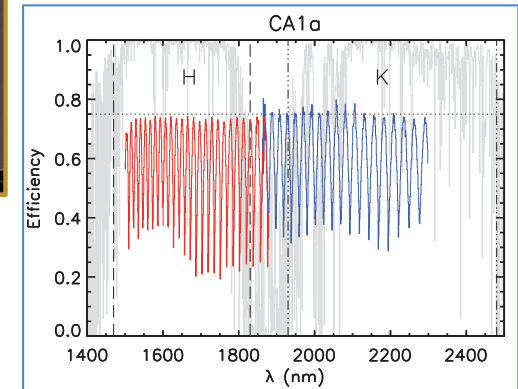
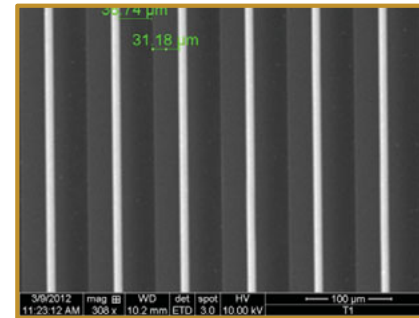
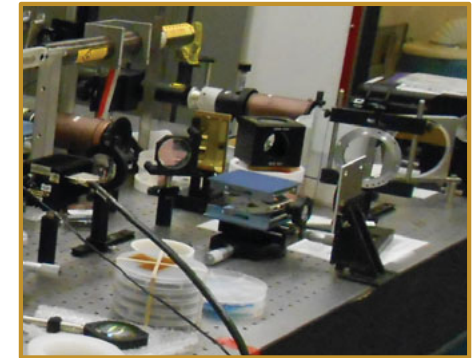


Aluminized Grating Surface



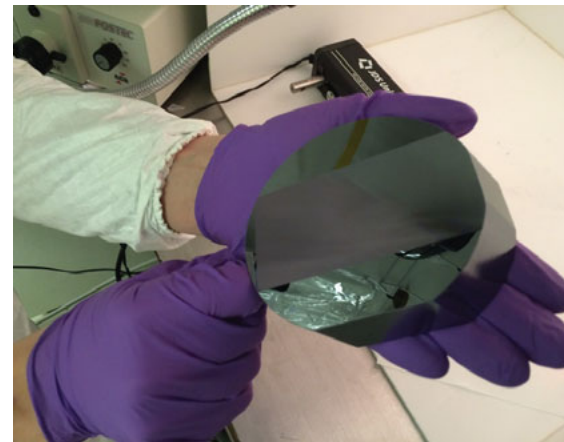
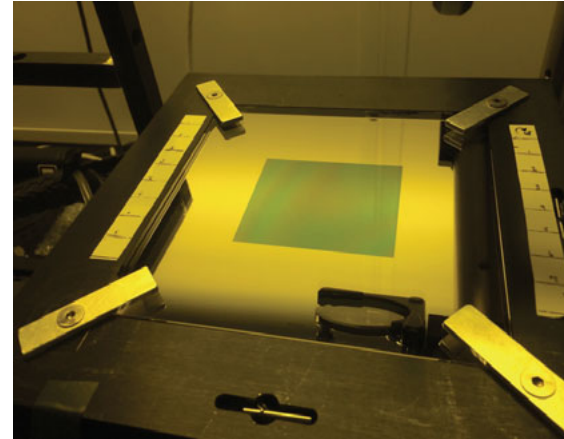
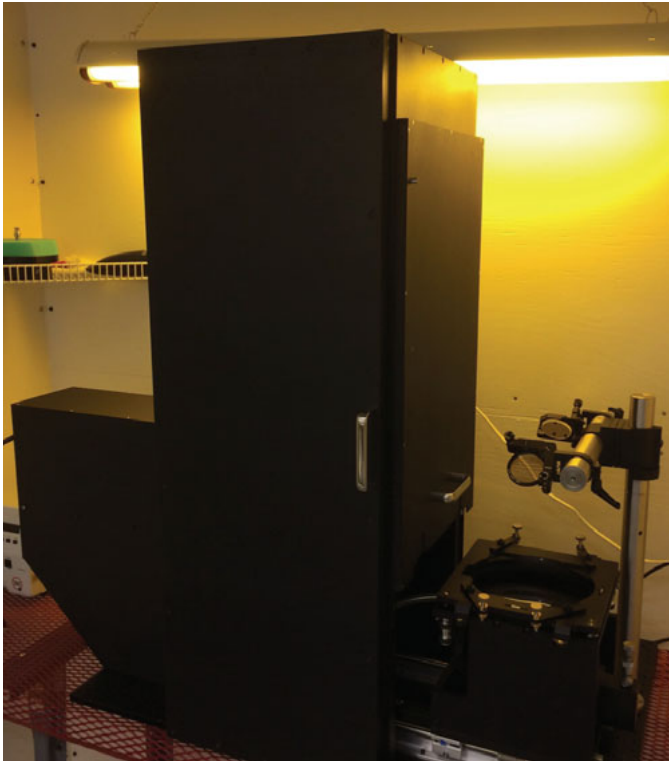
IGRINS immersion grating

Test	Specification
Front surface interferogram in Littrow at 633 nm (Equivalent to $\sim 2.15 \mu\text{m}$ in immersion)	$\lambda/4$ in immersion at operating wavelength
Laser spectrum	Ghosts $< 2 \times 10^{-3}$
Imaging with scanning electron microscope (SEM)	Smooth surface, $<< 1\%$ defect area
Efficiency in immersion over wavelength range	$\geq 75\%$

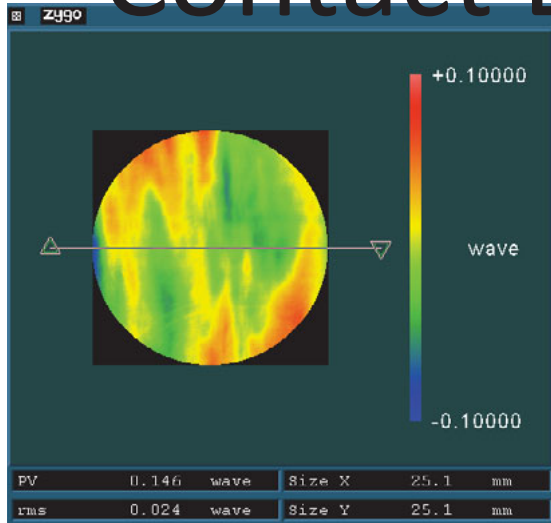


Contact Lithography

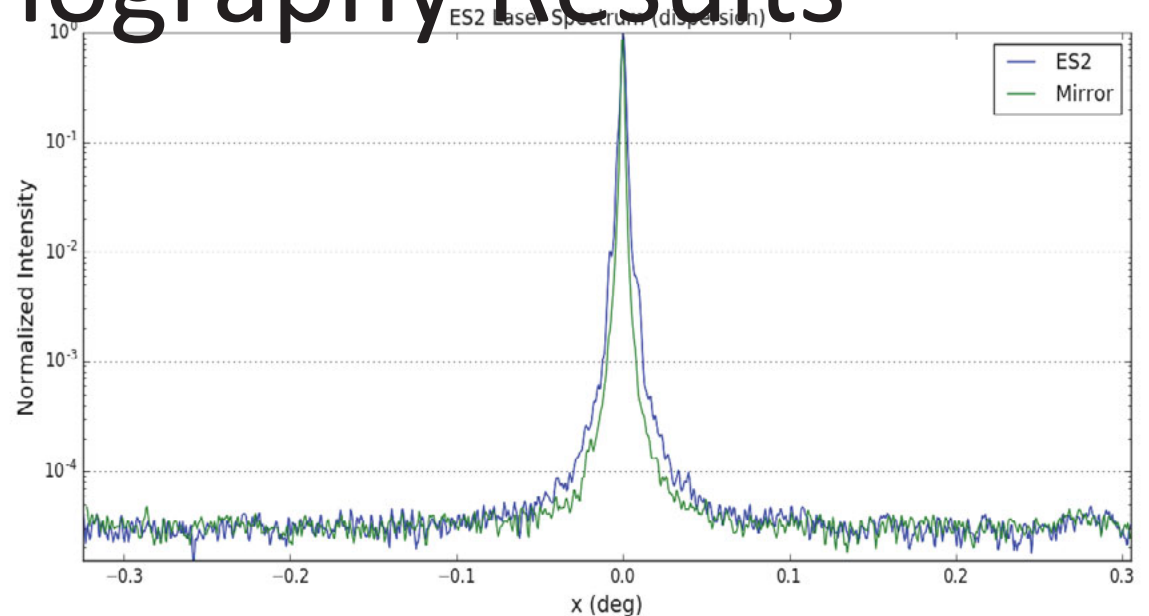
UTexas Grating Contact Aligner



Contact Lithography Results

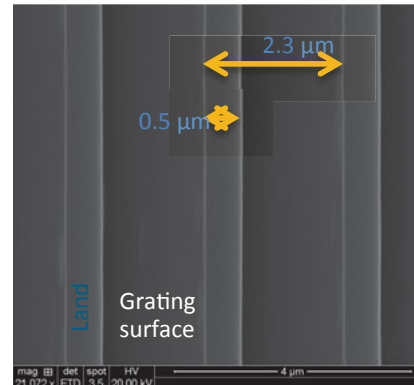
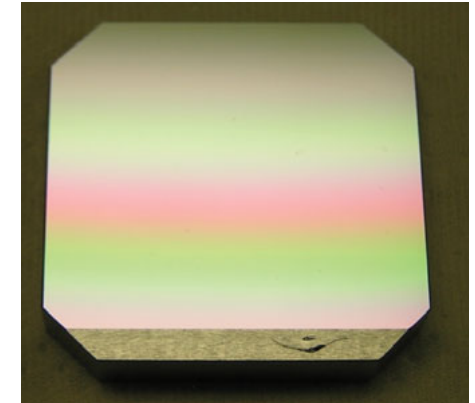
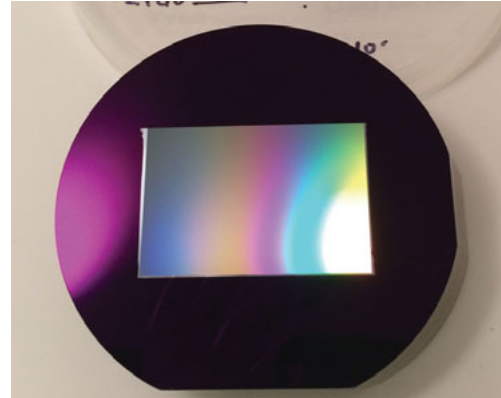


- Front surface interferogram in Littrow at 71.6° for a 25 mm beam.
- Phase PV is 0.146 waves at 633 nm, corresponding to $\sim 2.0 \mu\text{m}$ in immersion.

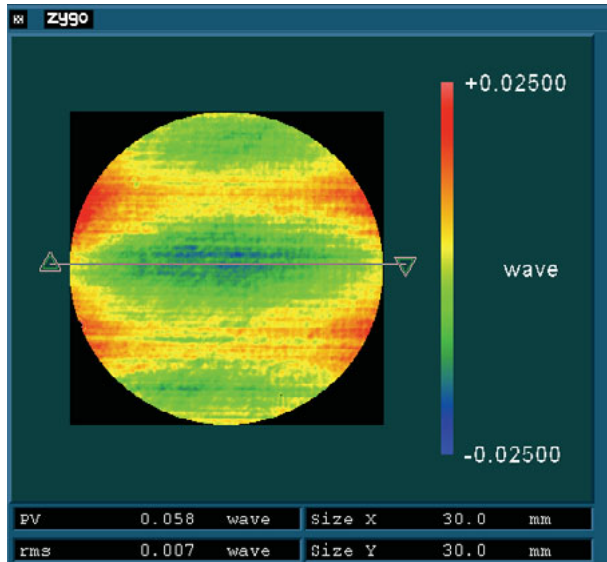


- High dynamic range, front surface monochromatic spectrum of same grating.
- Contact gratings can be as coarse as 5 l/mm

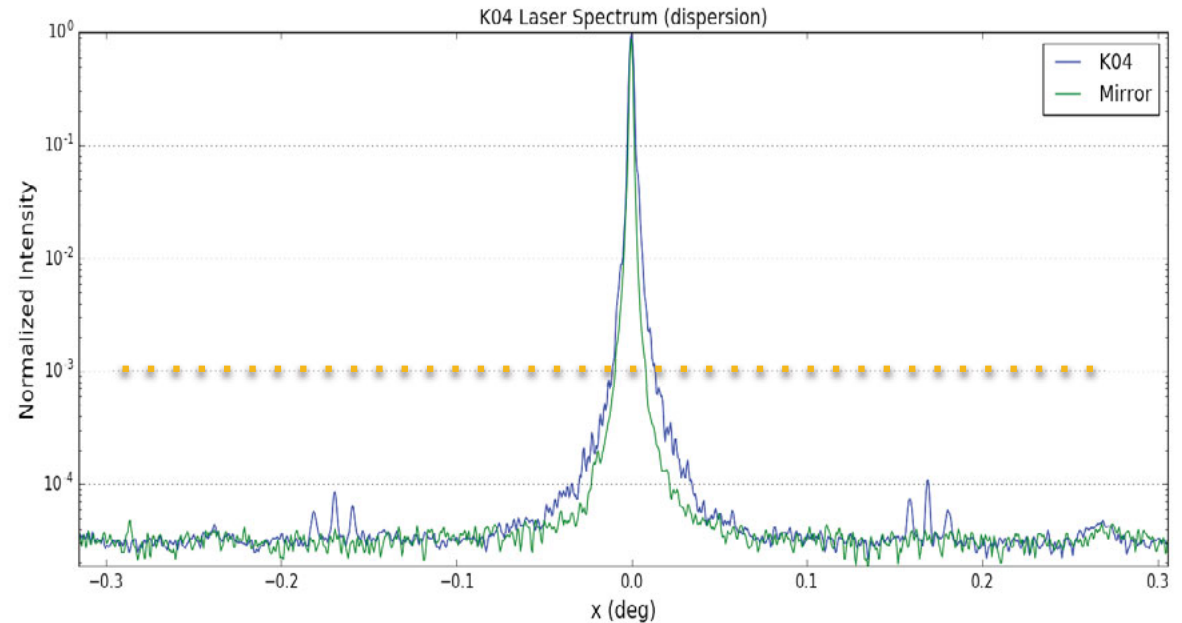
JPL electron beam lithography tool



Electron beam lithography allows us to make very fine-pitch gratings of 1 μm or below.



- Front surface interferogram in Littrow at 18° for a 30 mm beam.
- Phase PV is 0.06 waves at 633 nm, corresponding to $\sim 2.0 \mu\text{m}$ in immersion.



- High dynamic range, front surface monochromatic spectrum of same grating.
- Ghost specification is $<10^{-3}$ of the central peak; these are $<10^{-4}$.

Degree of Difficulty

Degree of difficulty: scales with $[(n-1) \sin\delta]/\lambda$ for grisms and with $[2n\sin\delta]/\lambda$ for immersion gratings. Scales with length of grating divided by width of slit in units of diffraction limited width.

Forcast grism 1: $\delta=11^\circ$ $\lambda= 30 \mu\text{m}$, DD=1

Other Forcast grisms: DD=1-10

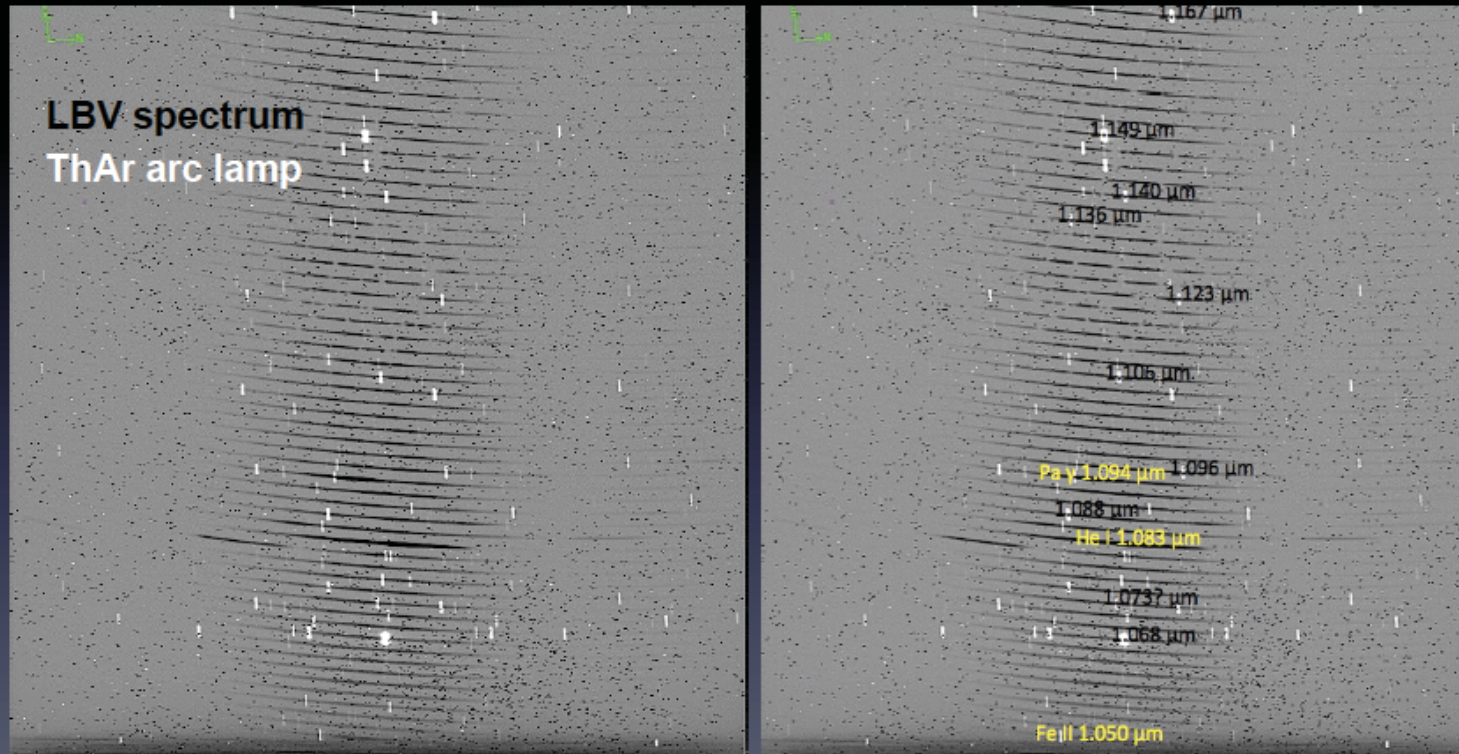
JWST grisms: DD= 9

IG for IGRINS: DD=120

IG for GMTNIRS: DD= 250



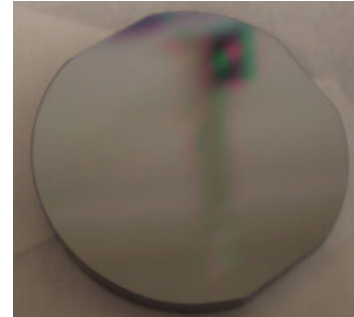
iSHELL: new J0 mode (for He I 1.083 μm)



At 80K Silicon transparent to full intensity at 1.065 μm
half intensity at 1.050 μm , zero intensity at 1.035 μm

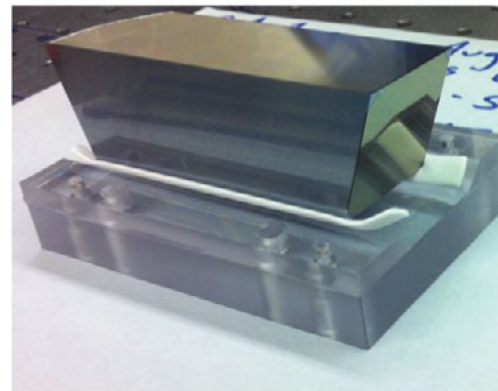
Silicon grism flight parts:

- James Webb Space Telescope NIRCam
- FORCAST on SOFIA Telescope

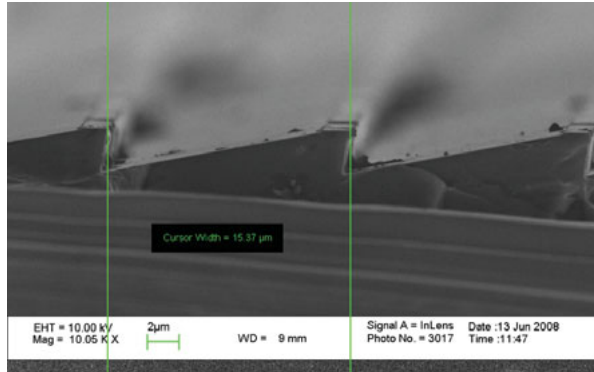


Echelle immersion gratings:

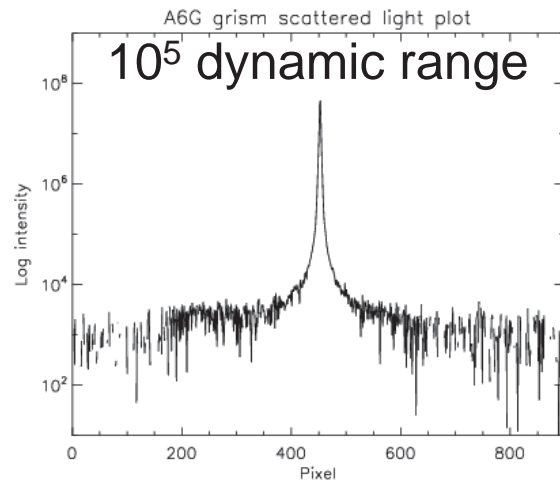
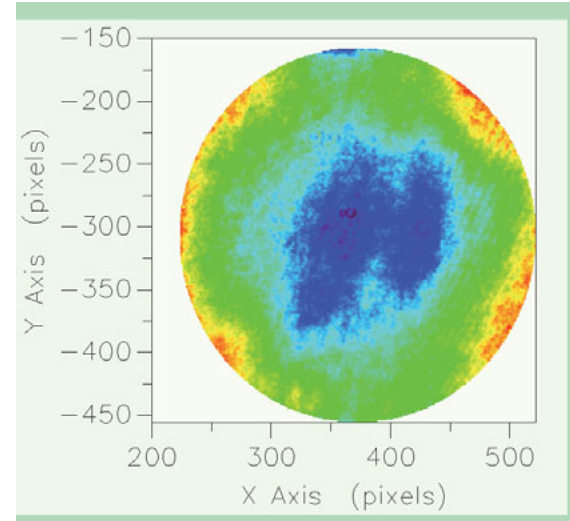
- Immersion GRating Infrared Spectrograph (IGRINS) installed at McDonald Observatory
- iShell for the NASA InfraRed Telescope Facility
- Planned GMT Near InfraRed Spectrograph (GMTNIRS) for the Giant Magellan Telescope.



JWST NIRCam Grisms



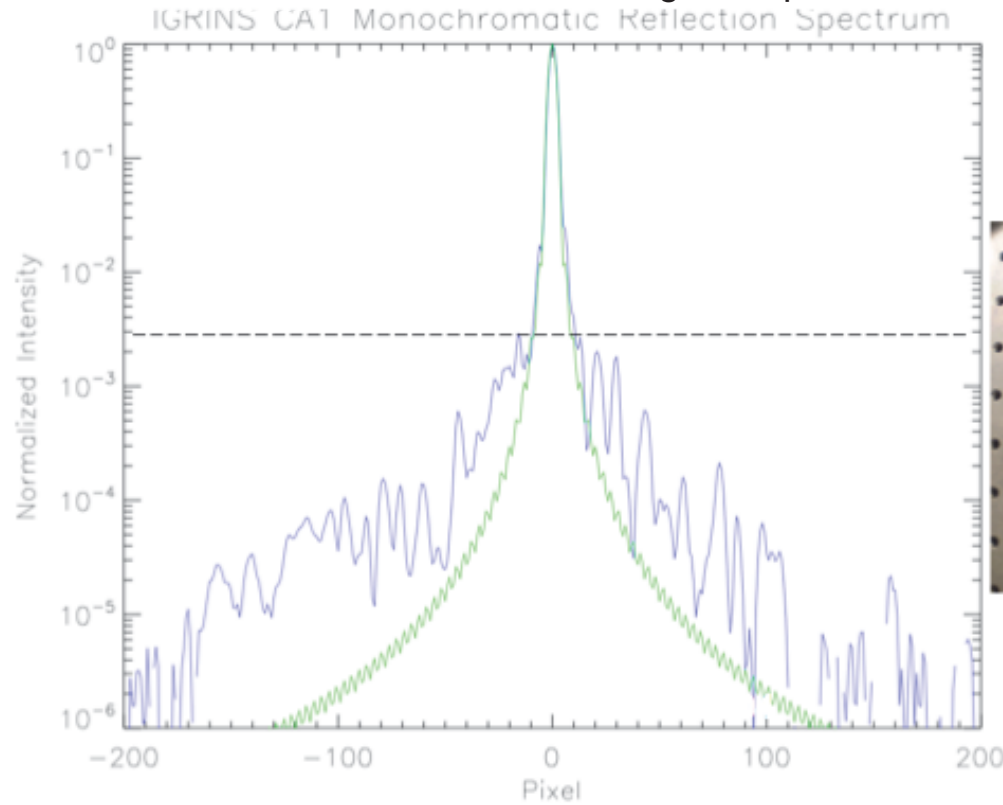
$\lambda/100$ rms grating surface



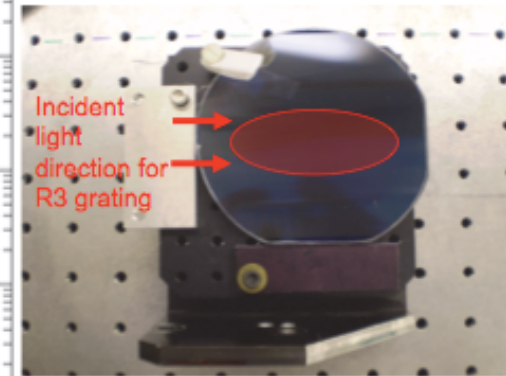
Flight Part



IGRINS Immersion Grating- Complete 2011



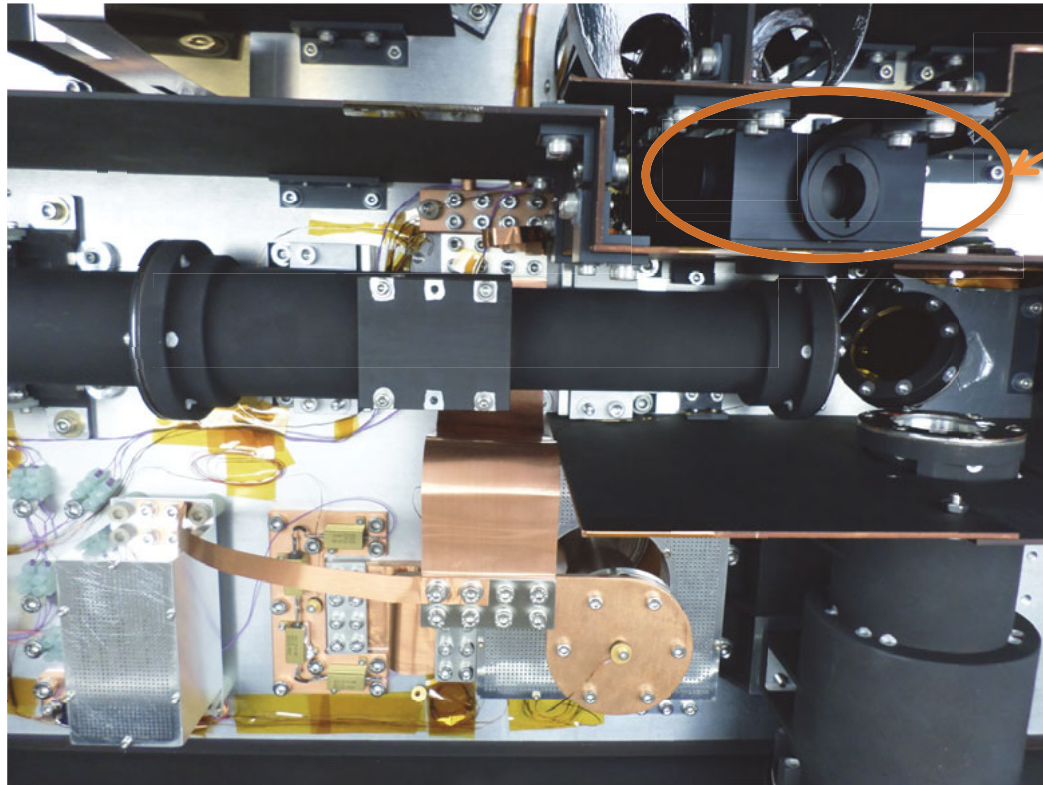
- wavelength - 543 nm
- beam size – 20 mm
- logarithm scale



Setup example for R3 grating

Green – theoretical line
Blue – measurement

Surface is $\lambda/6$ peak to valley. Efficiency ~80%

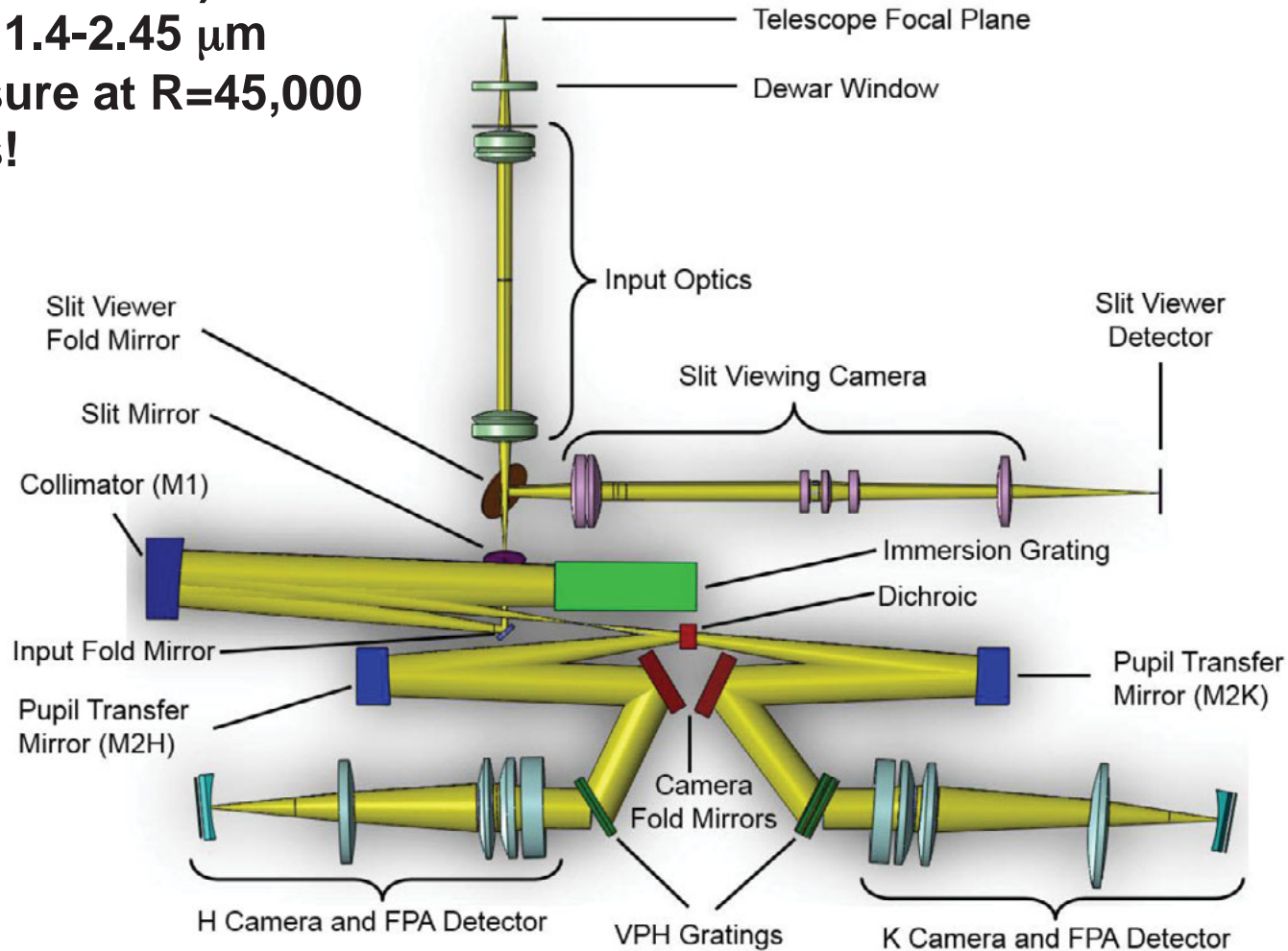


IGRINS
Immersion Grating

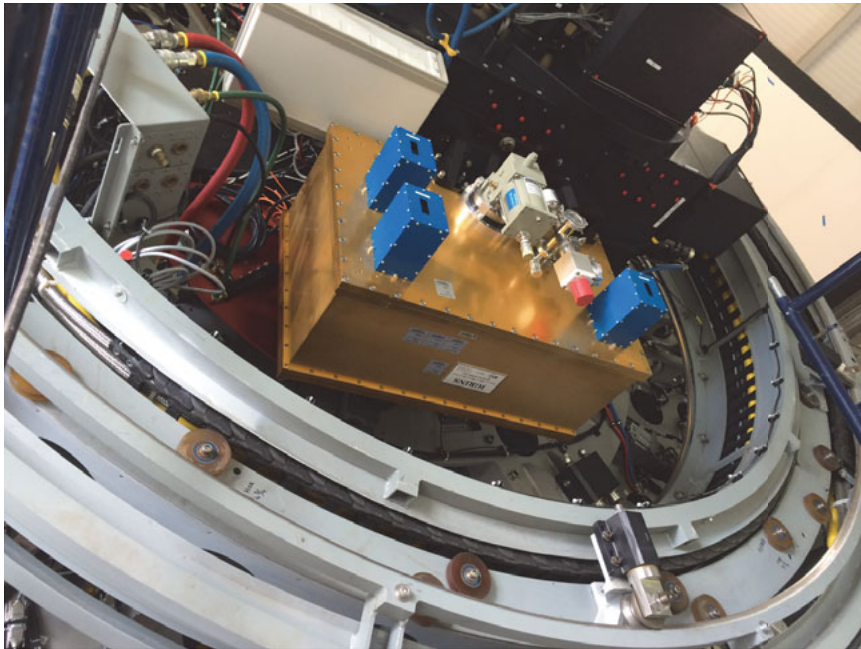
Infrared



IGRINS (UT and KASI)
covers all of 1.4-2.45 μm
in one exposure at $R=45,000$
with no gaps!

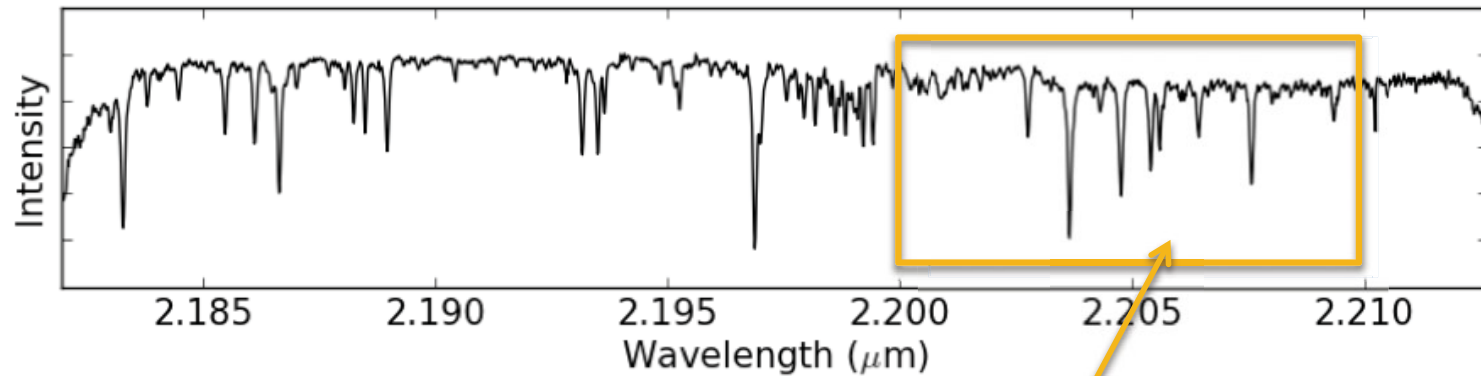
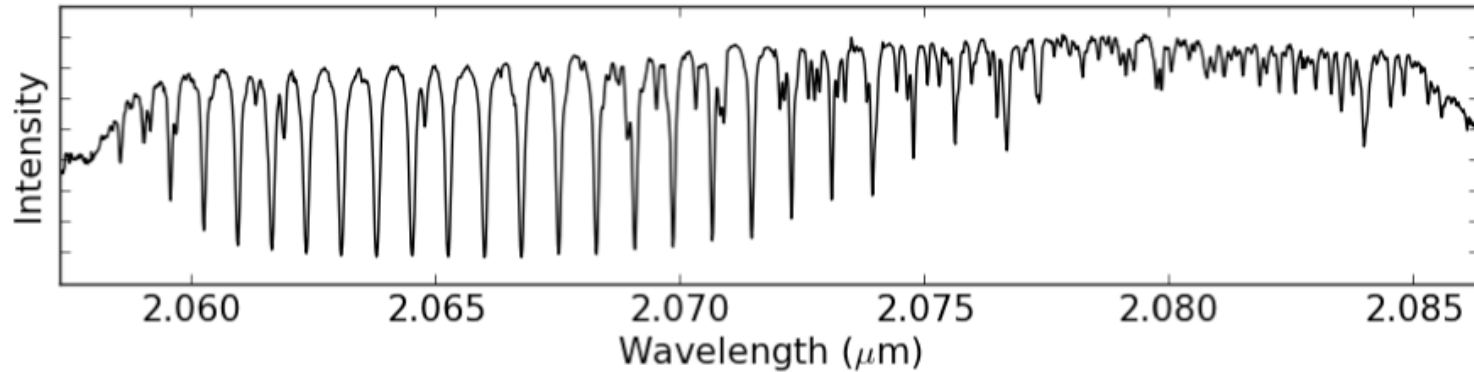


IGRINS on McDonald 2.7m
2014-2016, no cold moving parts,
warm calibration system with
moving mirrors

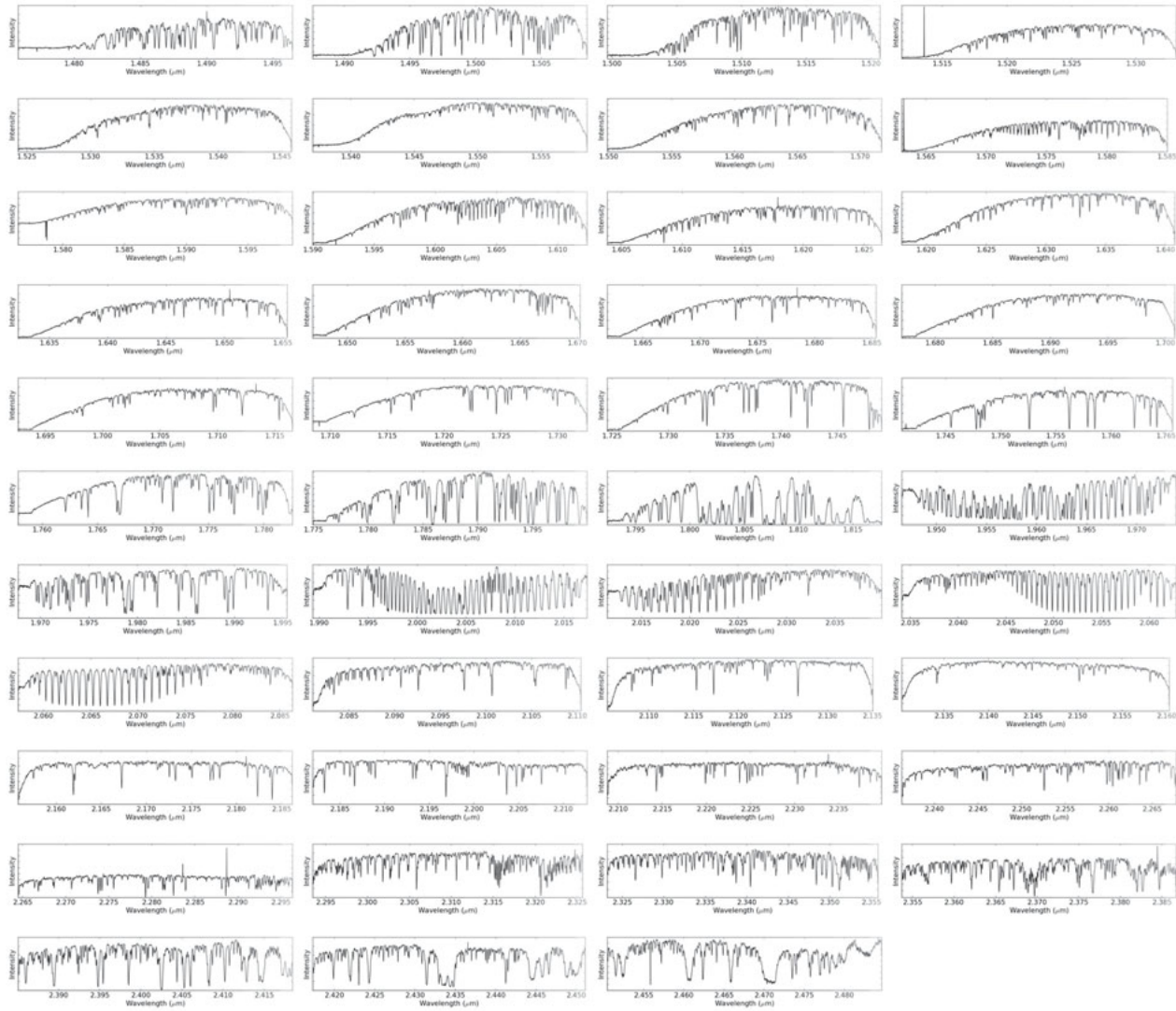


IGRINS on 4.3m DCT 2016- and
McDonald 2.7m 2017-
No moving parts, sky emission and
absorption lines, white spot

IGRINS Spectrum of a star, not corrected for telluric absorption



Region covered by the Phoenix spectrograph





TEXAS

The University of Texas at Austin

